

# EE 434

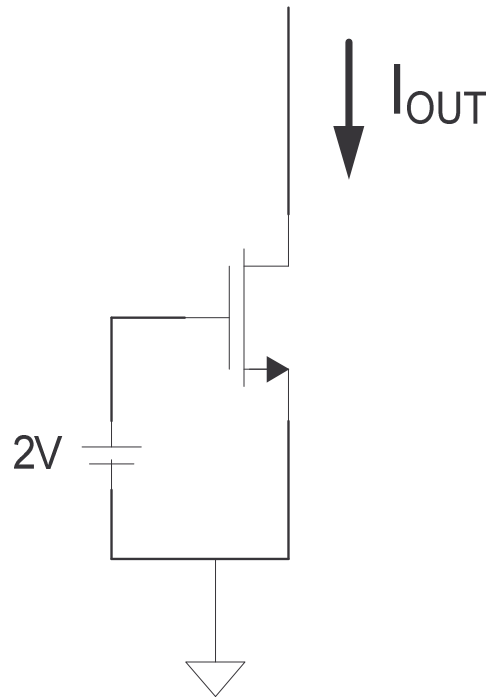
## Lecture 22

Properties of Bipolar Devices

## Quiz 16

A dc current source is shown. If the device has width  $W=50\mu$ , length  $L=1.2\mu$ ,  $\mu C_{ox}=100\mu A V^{-2}$ ,  $V_T=.75V$  and  $\lambda=.04V^{-1}$ , determine

- The nominal output current
- The small signal output impedance
- The minimum output voltage to maintain operation as a current source



And the number is ....

1            8            7            5            3  
6            9            4            2

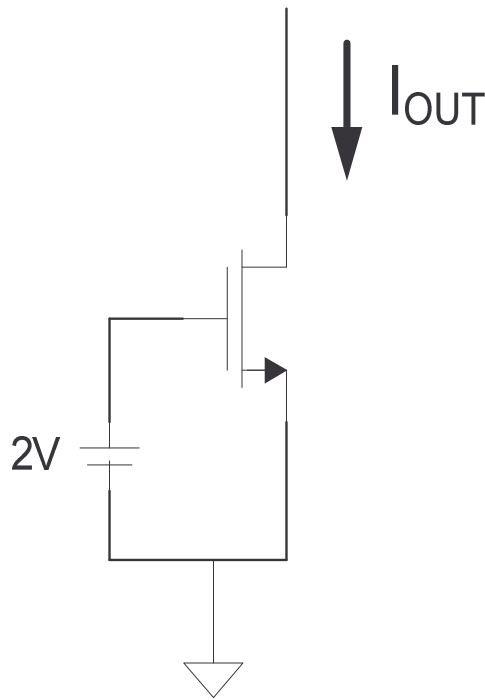
**7**

## Quiz 16

A dc current source is shown. If the device has width  $W=50\mu$ , length  $L=1.2\mu$ ,  $\mu C_{ox}=100\mu A V^{-2}$ ,  $V_T=.75V$  and  $\lambda=.04V^{-1}$ , determine

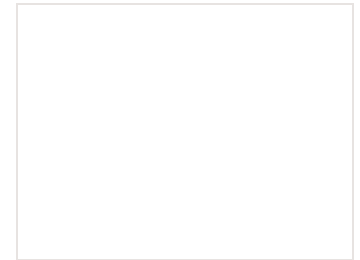
- The nominal output current
- The small signal output impedance
- The minimum output voltage to maintain operation as a current source

### Solution



$$I_{DQ} \cong \mu C_{OX} \frac{W}{2L} (V_{EB})^2$$

$$I_{DQ} \cong 10^{-4} \frac{50}{2 \cdot 1.2} (2 - .75)^2 mA$$

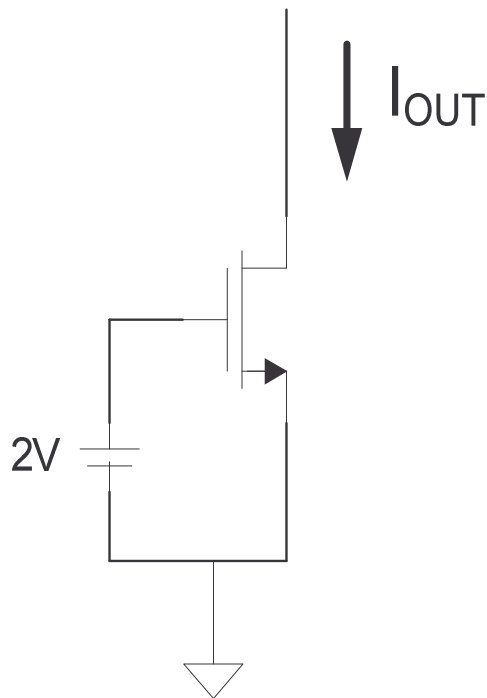


## Quiz 16

A dc current source is shown. If the device has width  $W=50\mu$ , length  $L=1.2\mu$ ,  $\mu C_{ox}=100\mu A V^{-2}$ ,  $V_T=.75V$  and  $\lambda=.04V^{-1}$ , determine

- The nominal output current
- The small signal output impedance
- The minimum output voltage to maintain operation as a current source

## Solution



$$I_{DQ} \cong \mu C_{OX} \frac{W}{2L} (V_{EB})^2$$

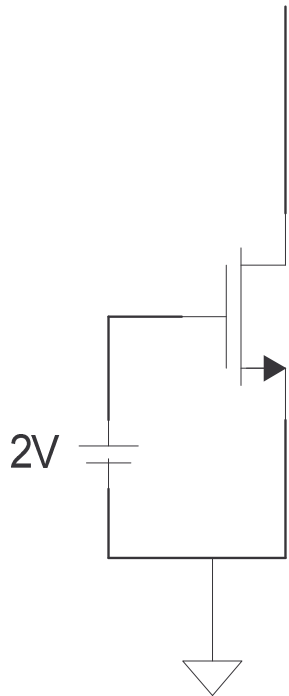
$$I_{DQ} \cong 10^{-4} \frac{50}{2 \cdot 1.2} (2 - .75)^2 mA = 3.25 mA$$

## Quiz 16

A dc current source is shown. If the device has width  $W=50\mu$ , length  $L=1.2\mu$ ,  $\mu C_{ox}=100\mu A V^{-2}$ ,  $V_T=.75V$  and  $\lambda=.04V^{-1}$ , determine

- The nominal output current
- The small signal output impedance
- The minimum output voltage to maintain operation as a current source

### Solution



$$R_{OUT} = \frac{1}{g_o}$$

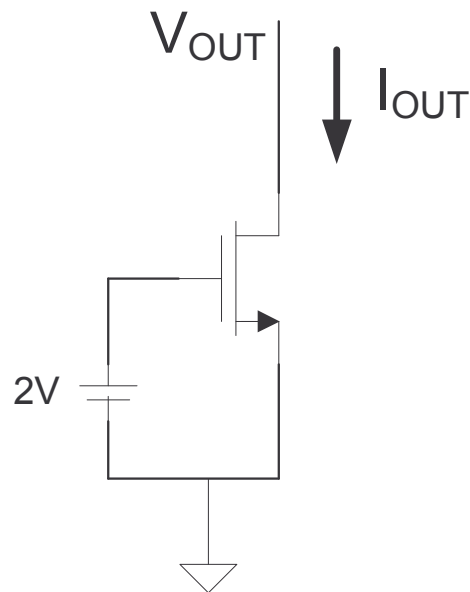
$$R_{OUT} = \frac{1}{\lambda I_{DQ}} = \frac{1}{.04V^{-1} \cdot 3.25mA} = 7.7K\Omega$$

## Quiz 16

A dc current source is shown. If the device has width  $W=50\mu$ , length  $L=1.2\mu$ ,  $\mu C_{ox}=100\mu A V^{-2}$ ,  $V_T=.75V$  and  $\lambda=.04V^{-1}$ , determine

- The nominal output current
- The small signal output impedance
- The minimum output voltage to maintain operation as a current source

## Solution



To maintain saturation region operation,  $V_{DS} > V_{GS} - V_T$

$$V_{OUT} > 2V - .75V = 1.25V$$

## Review from Last Time

Alternate equivalent small signal model for BJT includes current dependent current source as alternative to transconductance source

For a bipolar transistor

$$\mathbf{g_m} \gg \mathbf{g_{\pi}} \gg \mathbf{g_o}$$

$g_m$  for the BJT is much larger than that of the MOSFET (good)

$g_{\pi}$  for BJT is much larger than that of the MOSFET (not so good)



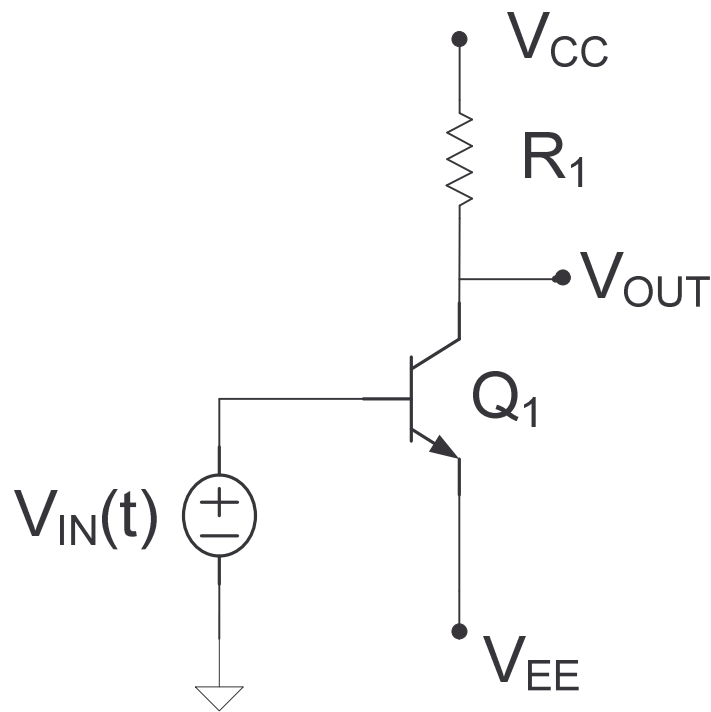
# Other Properties of BJT

- Alternate Equivalent Small Signal Model
- Relative magnitude of small signal parameters
  - Simplified small signal model

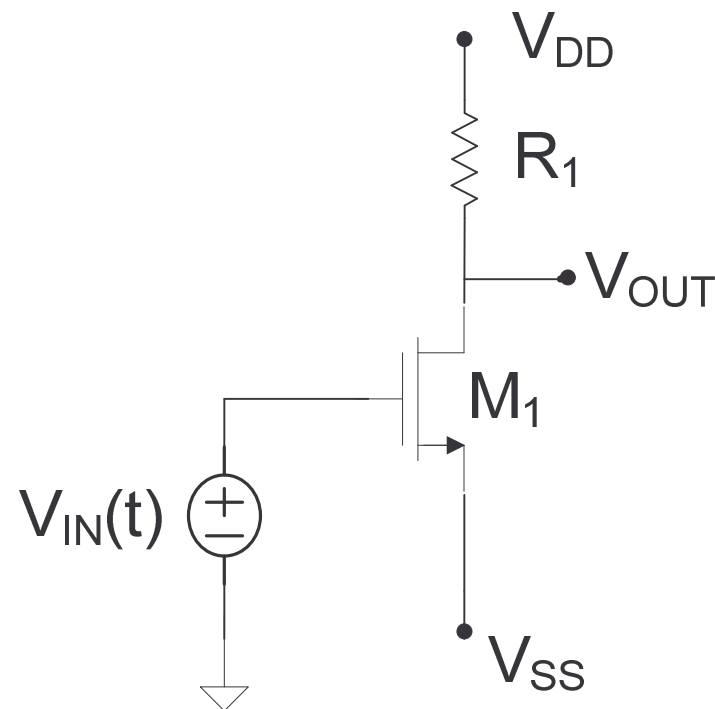
 Comparison of BJT and MOSFET

# Comparison of MOSFET and BJT

## BJT



## MOSFET



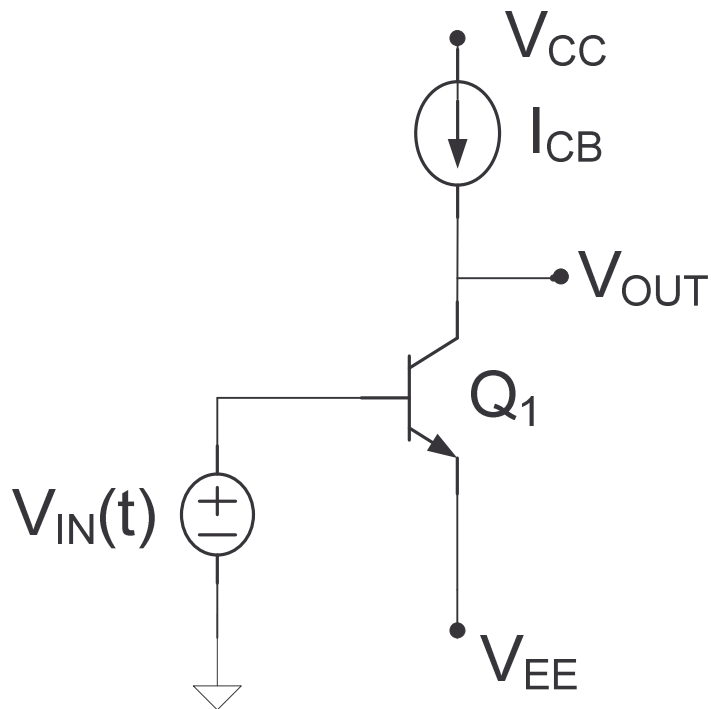
Assume BJT operating in FA region, MOSFET operating in Saturation

Assume same quiescent output voltage and same resistor  $R_1$

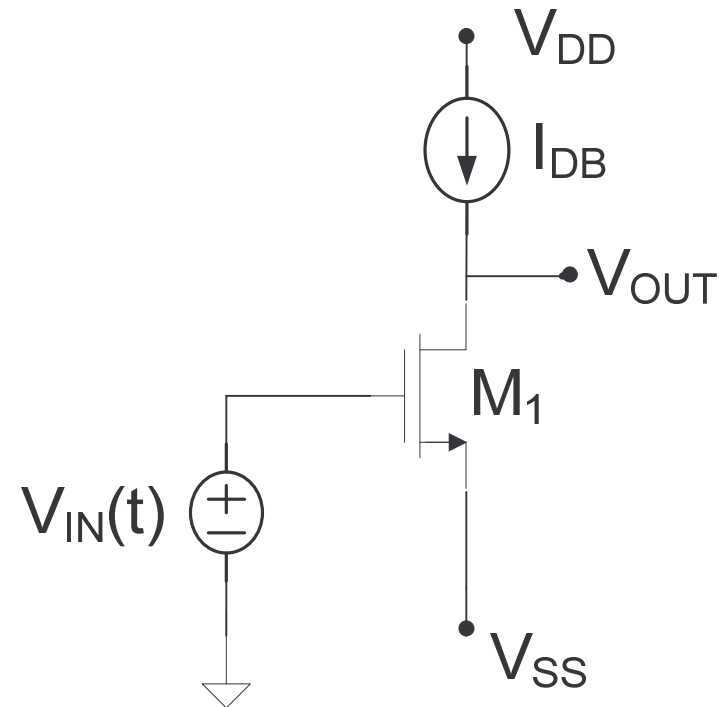
One of the most widely used amplifier architectures

# Comparison of MOSFET and BJT

## BJT



## MOSFET

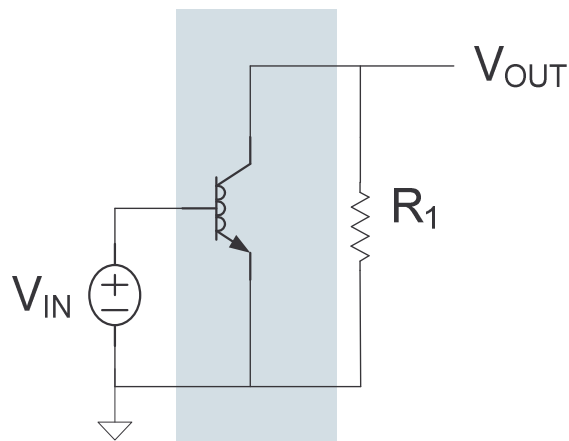
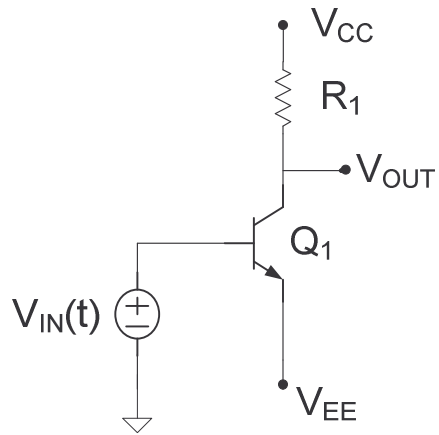


Assume BJT operating in FA region, MOSFET operating in Saturation  
Assume same bias current

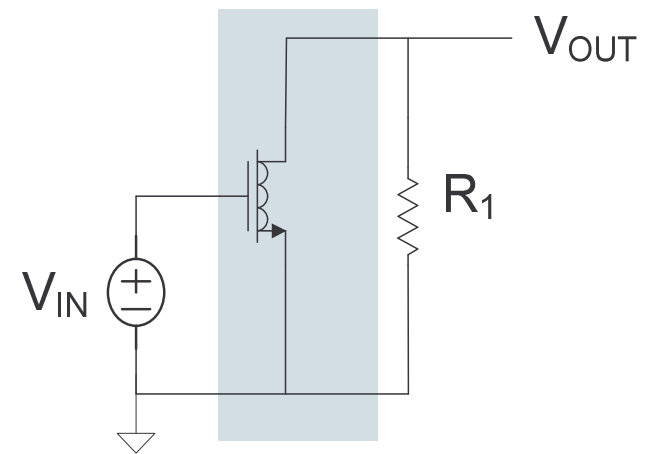
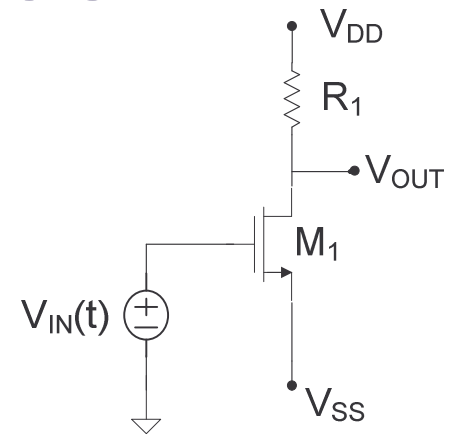
One of the most widely used amplifier architectures in integrated applications  
Special Case of Previous Architecture

# Comparison of MOSFET and BJT

## BJT

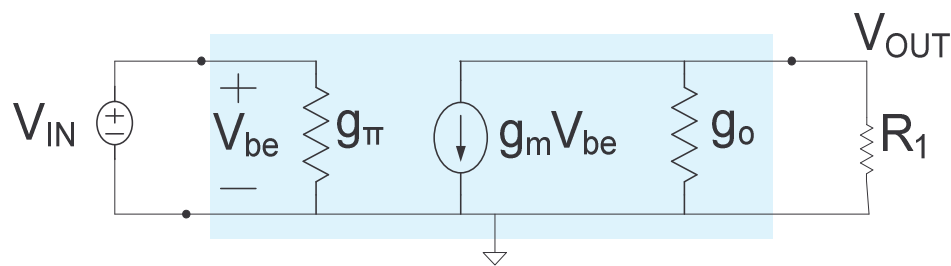
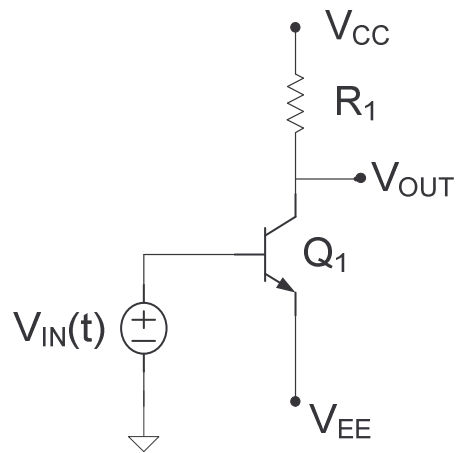


## MOSFET

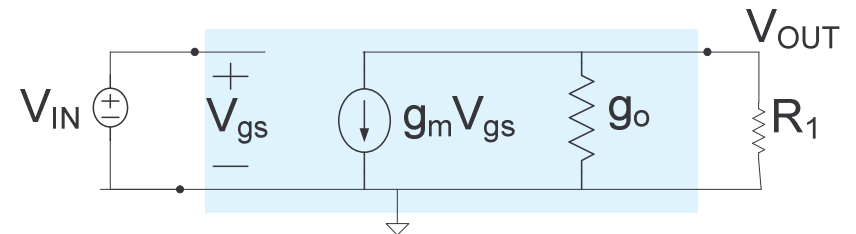
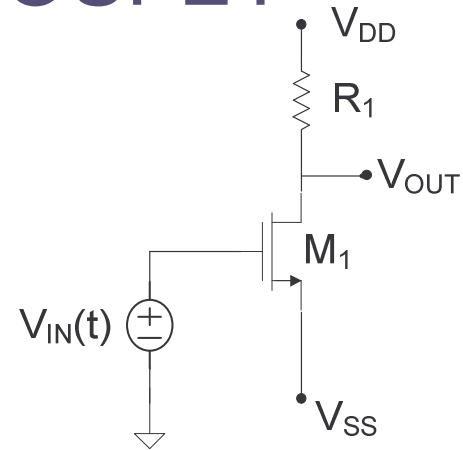


# Comparison of MOSFET and BJT

## BJT

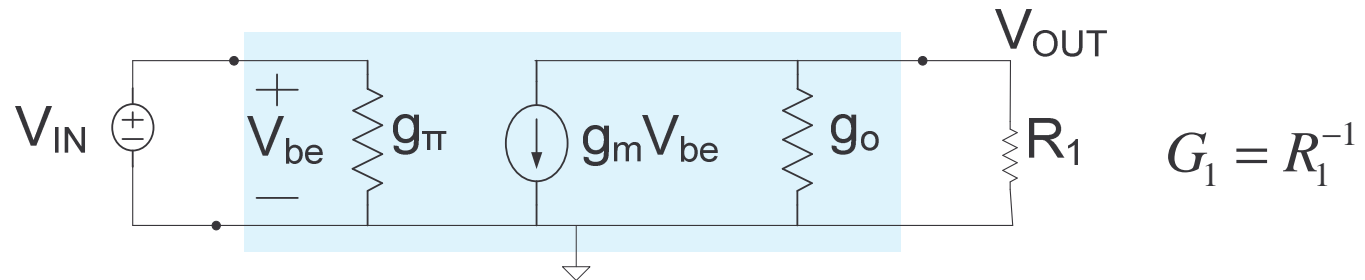


## MOSFET



# Comparison of MOSFET and BJT

## BJT



$$v_{OUT} = -\frac{g_m}{g_o + G_1} v_{IN}$$

$$A_V = \frac{v_{OUT}}{v_{IN}} = -\frac{g_m}{g_o + G_1}$$

$$v_{OUT} \cong -\frac{g_m}{G_1} v_{IN}$$

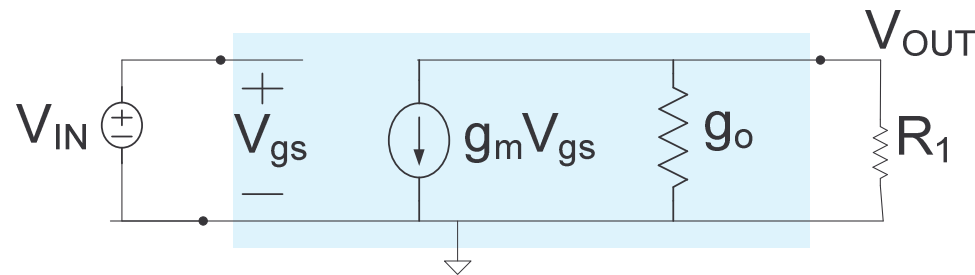
$$A_V = \frac{V_{OUT}}{V_{IN}} = -g_m R_1$$

$$g_m = \frac{I_{CQ}}{V_t}$$

$$A_V = -\frac{I_{CQ} R_1}{V_t}$$

# Comparison of MOSFET and BJT

## MOSFET



$$G_1 = R_1^{-1}$$

$$v_{OUT} = -\frac{g_m}{g_o + G_1} v_{IN}$$

$$A_V = \frac{v_{OUT}}{v_{IN}} = -\frac{g_m}{g_o + G_1}$$

$$v_{OUT} \cong -\frac{g_m}{G_1} v_{IN}$$

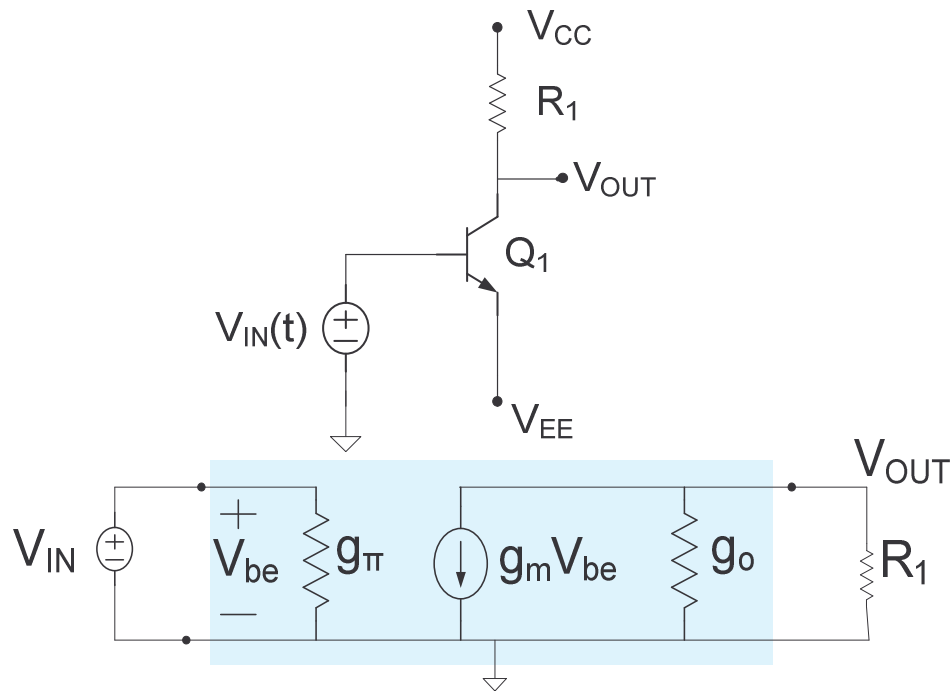
$$A_V = \frac{V_{OUT}}{V_{IN}} = -g_m R_1$$

$$g_m = \frac{2I_{DQ}}{V_{EB}}$$

$$A_V = -\frac{2I_{DQ}R_1}{V_{EB}}$$

# Comparison of MOSFET and BJT

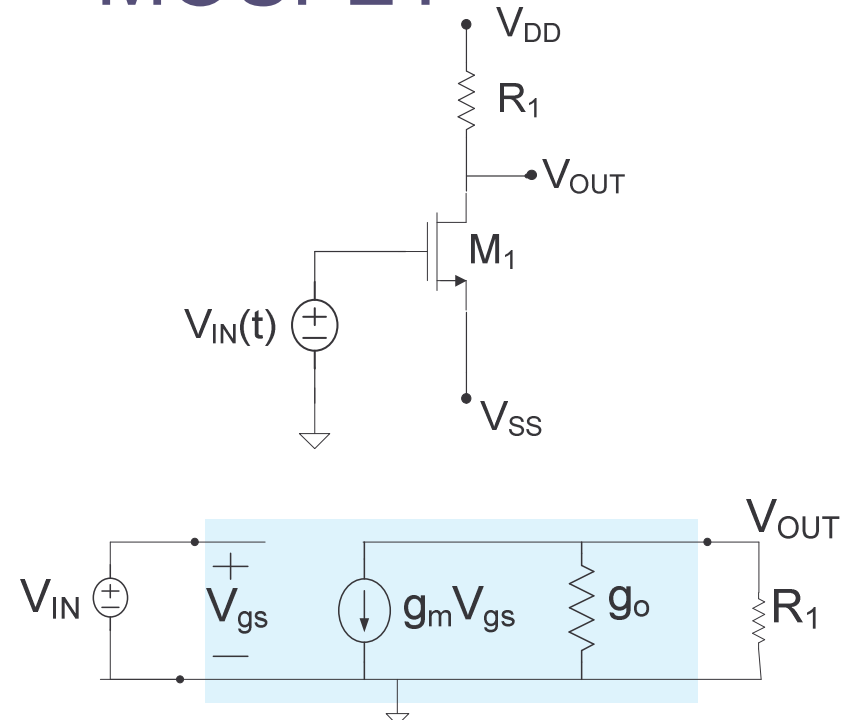
## BJT



$$A_{VB} = -\frac{I_{CQ} R_1}{V_t}$$

$$\frac{A_{VB}}{A_{VM}} = \frac{V_{EB}}{2V_t}$$

## MOSFET



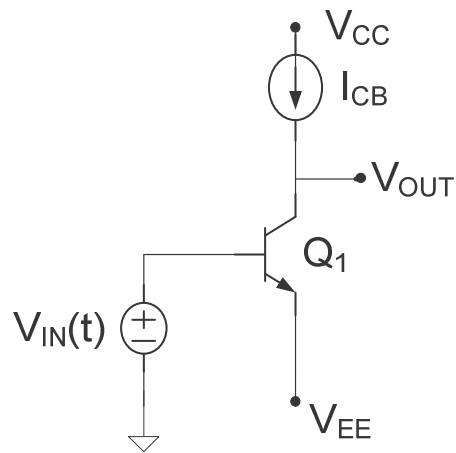
$$A_{VM} = -\frac{2I_{DQ} R_1}{V_{EB}}$$

$A_{VB}$  is typically much larger than  $A_{VM}$  for this basic amplifier architecture

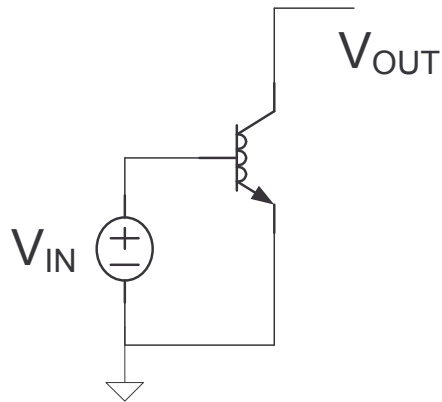


# Comparison of MOSFET and BJT

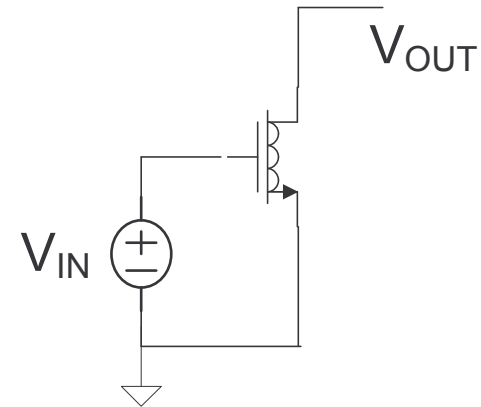
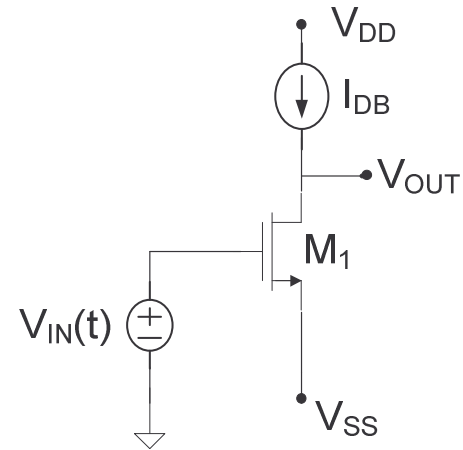
## BJT



Assume same bias currents

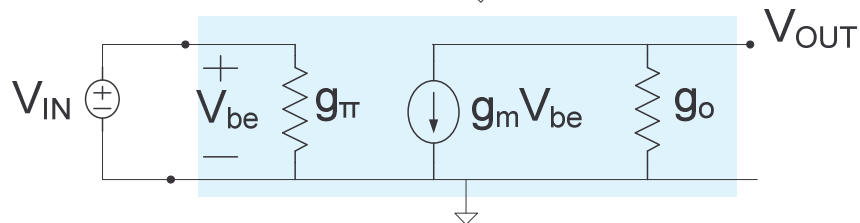
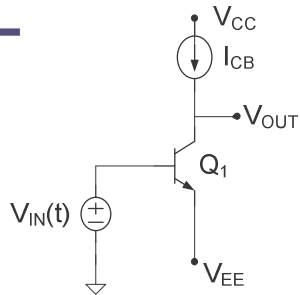


## MOSFET



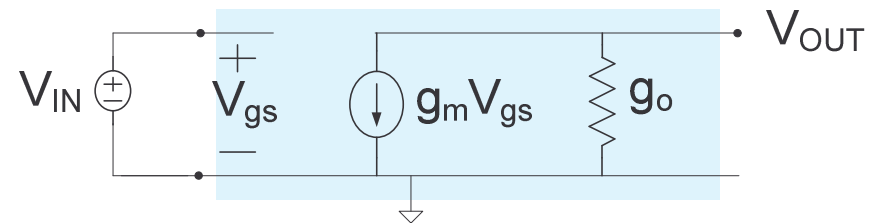
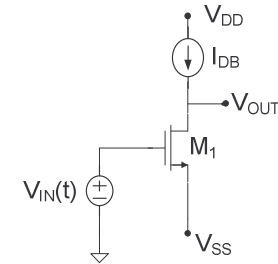
# Comparison of MOSFET and BJT

BJT



$$A_V = \frac{V_{OUT}}{V_{IN}} = -\frac{g_m}{g_o}$$

MOSFET



$$A_V = \frac{V_{OUT}}{V_{IN}} = -\frac{g_m}{g_o}$$

Identical functional form

$$\frac{A_{VB}}{A_{VM}} = \frac{\left[ \frac{g_{mB}}{g_{oB}} \right]}{\left[ \frac{g_{mM}}{g_{oM}} \right]} = \left[ \frac{g_{mB}}{g_{mM}} \right] \left[ \frac{g_{oM}}{g_{oB}} \right]$$

Assuming same bias currents

$$\frac{A_{VB}}{A_{VM}} = \left[ \frac{V_{EB}}{2V_t} \right] [\lambda V_{AF}]$$

Typically  $A_{VB} \gg A_{VM}$

# Comparison of MOSFET and BJT

How do the areas required for implementing a MOSFET compare to those required for a BJT

To make the comparison fair, will assume the same lithography equipment and that the minimum feature size both processes is  $2\lambda$

Refer the design rules for a bipolar process in the GAS text if additional details are needed

The following slides are adapted from the BJT technology presentation

mid-line of isolation

1 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75

$63\lambda$

5

10

15

20

25

30

35

40

45

50

55

base diffusion

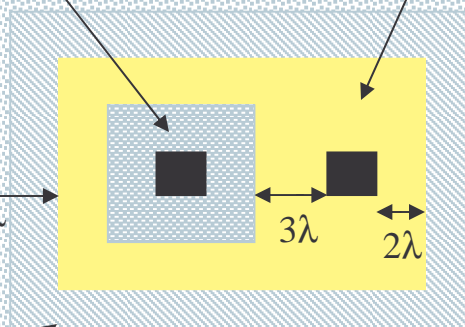
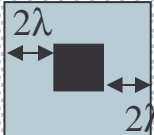
Emitter diffusion

$62\lambda$

$12\lambda$

$14\lambda$

$58\lambda$



Note:  $24\lambda$  required  
Between p-base and  
isolation diffusion

buried collector

n-epi

Minimum spacings for BJT (top view)

Isolation diffusion

mid-line of isolation

1 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75

5

10

15

20

25

30

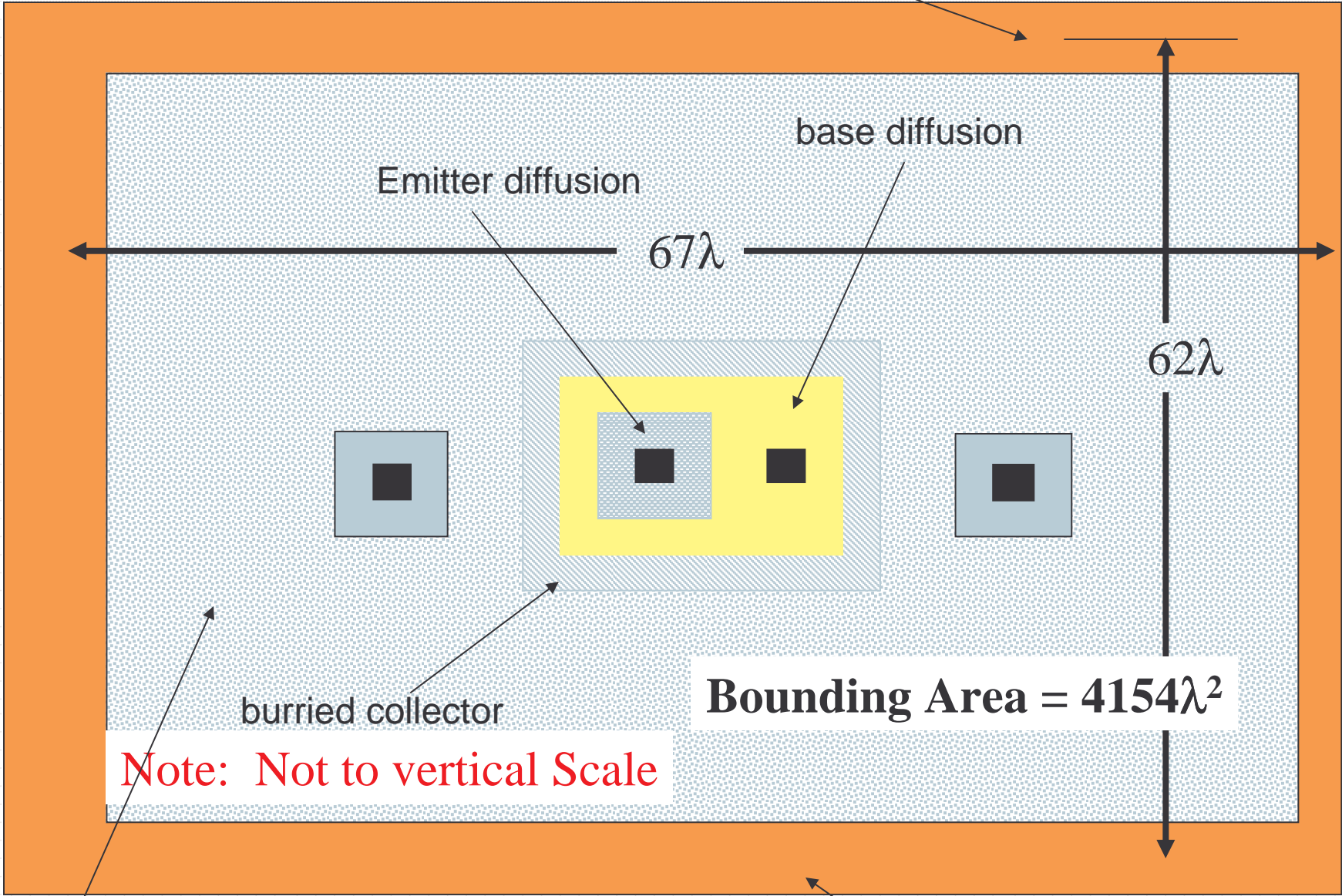
35

40

45

50

55



base diffusion

Emitter diffusion

$67\lambda$

$62\lambda$

buried collector

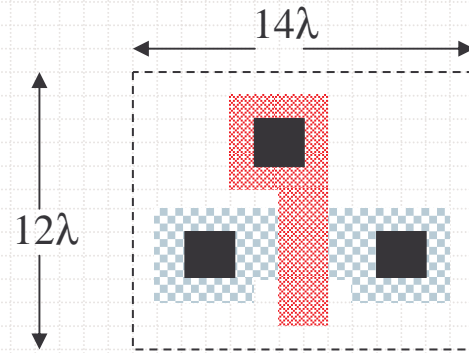
**Bounding Area = 4154λ<sup>2</sup>**

**Note: Not to vertical Scale**

n-epi

Isolation diffusion

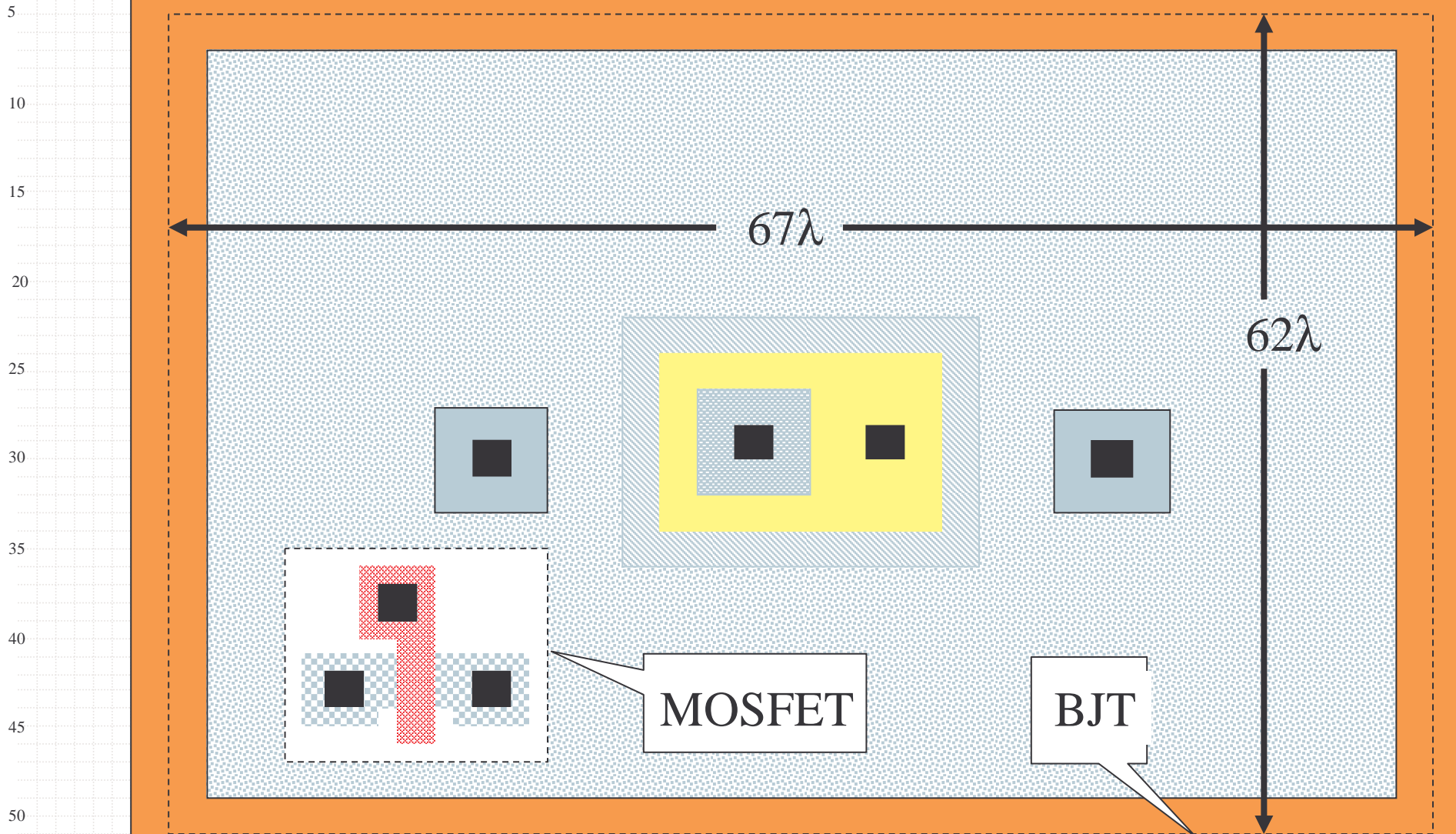
# Minimum-Sized MOSFET



Bounding Area =  $168\lambda^2$

Active Area =  $6\lambda^2$

1 5 10 15 20 25 30 35 40 45 50 55 60 65 70 75



Note: Not to vertical Scale

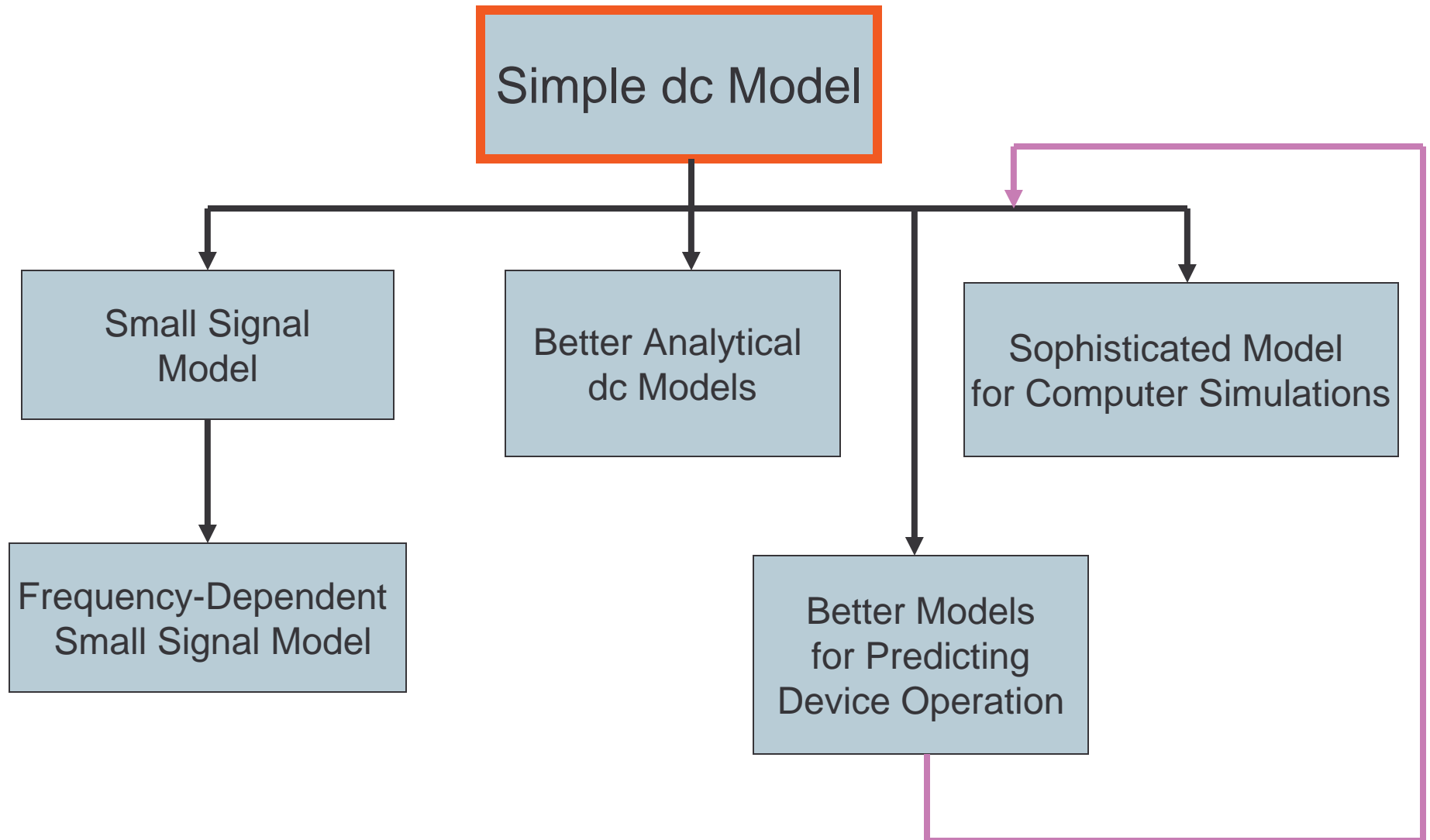
55

# Other Properties of BJT

- Alternate Equivalent Small Signal Model
  - Relative magnitude of small signal parameters
    - Simplified small signal model
  - Comparison of BJT and MOSFET
- ➔ Equivalent Circuit for dc biasing

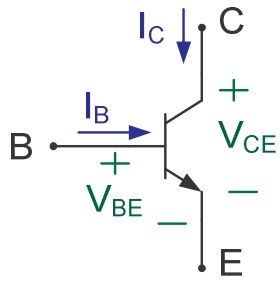


# Bipolar Models



# Bipolar Models

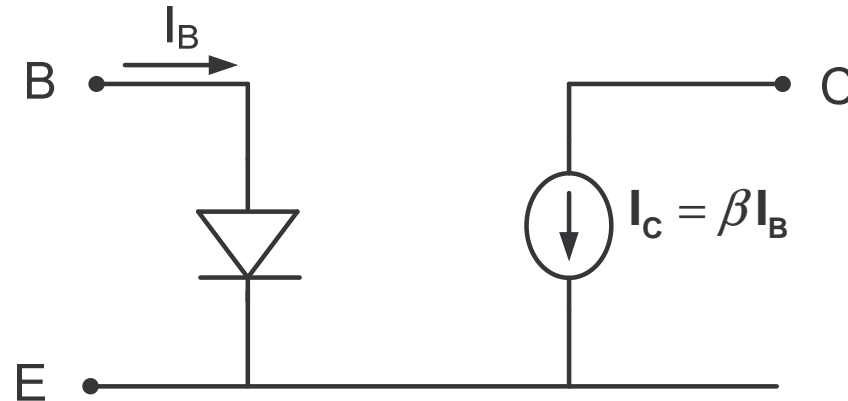
## Simple dc Model for Biasing



$$I_B = \frac{J_S A_E}{\beta} e^{\frac{V_{BE}}{V_t}}$$

$$I_C = J_S A_E e^{\frac{V_{BE}}{V_t}}$$

$$I_C = \beta I_B$$

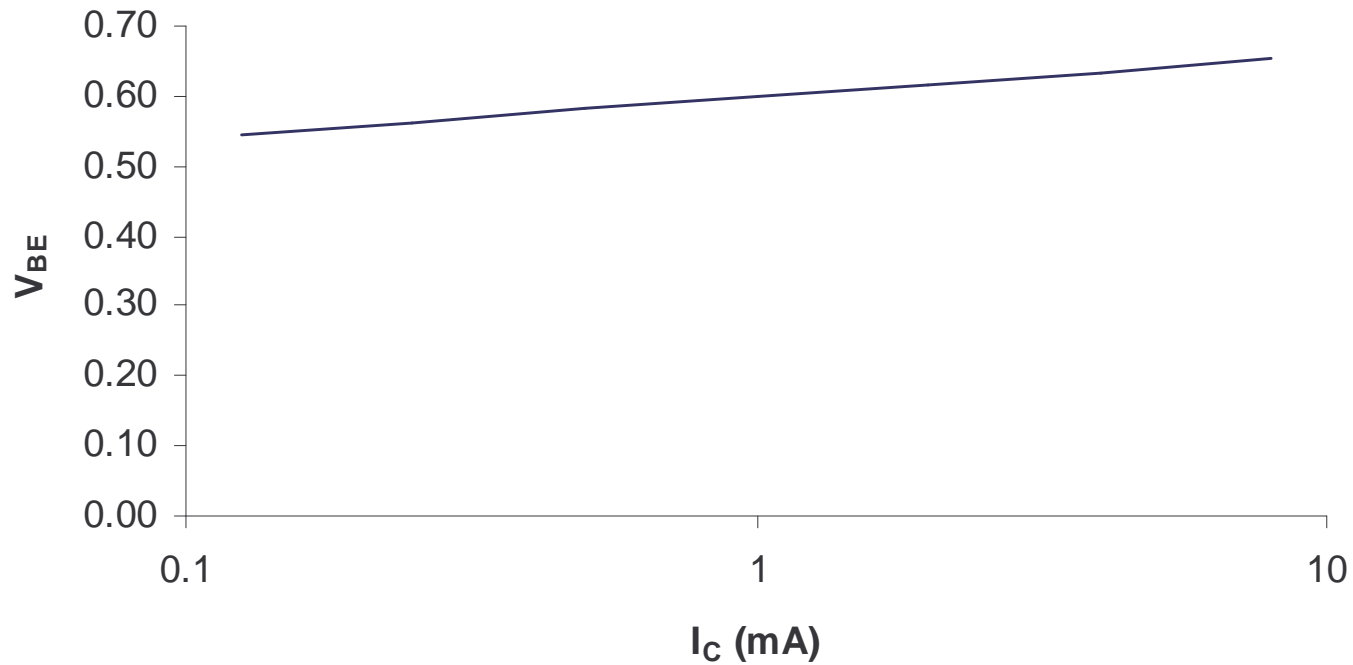


Although it may appear this is a model simplification, it is still highly nonlinear because the diode from BE is nonlinear

Recall

# Transfer Characteristics

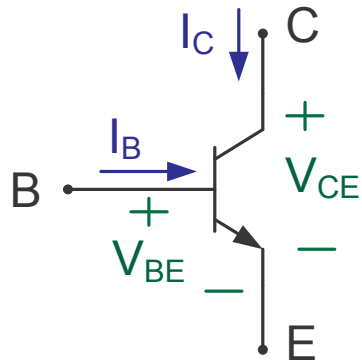
$$J_S = .25 \text{ fA}/\mu^2$$
$$A_E = 400 \mu^2$$



$V_{BE}$  close to 0.6V for a two decade change in  $I_C$  around 1mA

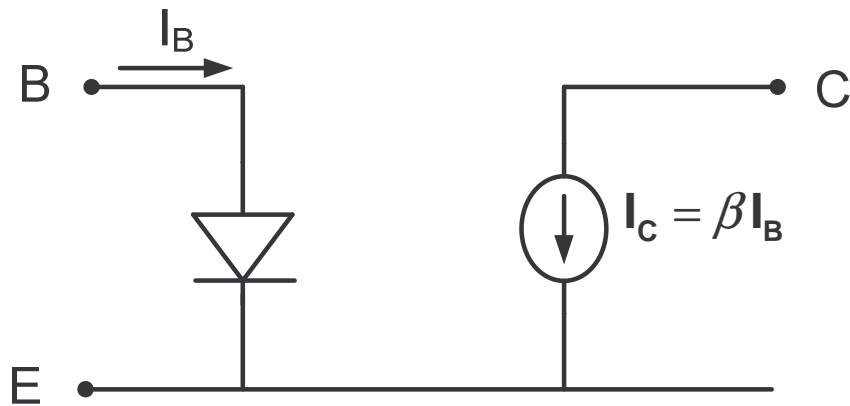
# Bipolar Models

Simple dc Model for Biasing



$$I_B = \frac{J_S A_E}{\beta} e^{\frac{V_{BE}}{V_t}}$$

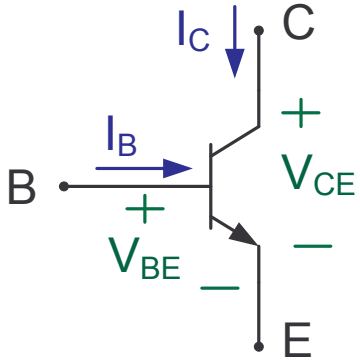
$$I_C = \beta I_B$$



$V_{BE}$  is approximately 0.6V when in FA region

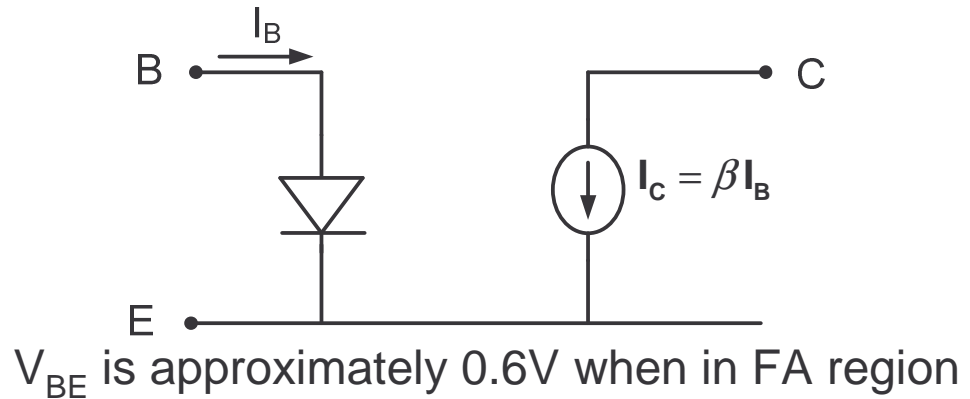
# Bipolar Models

Simple dc Model for Biasing



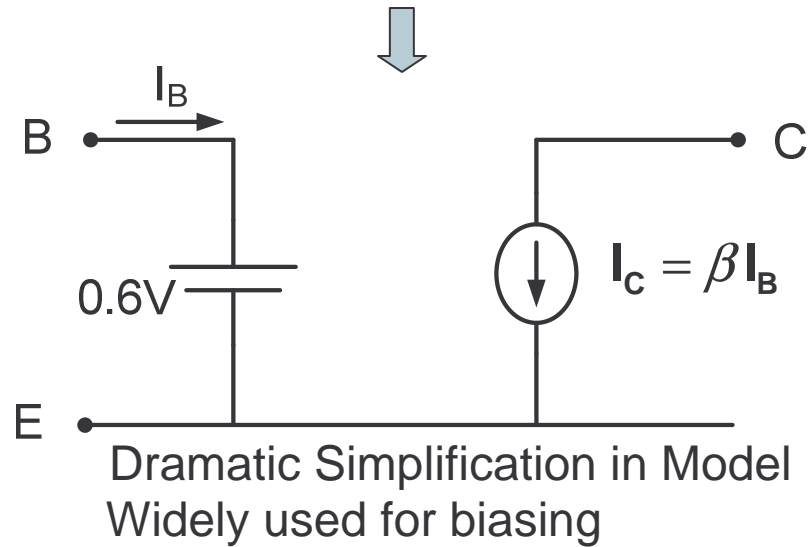
$$I_B = \frac{J_S A_E}{\beta} e^{\frac{V_{BE}}{V_t}}$$

$$I_C = \beta I_B$$



$$V_{BE} = 0.6V$$

$$I_C = \beta I_B$$

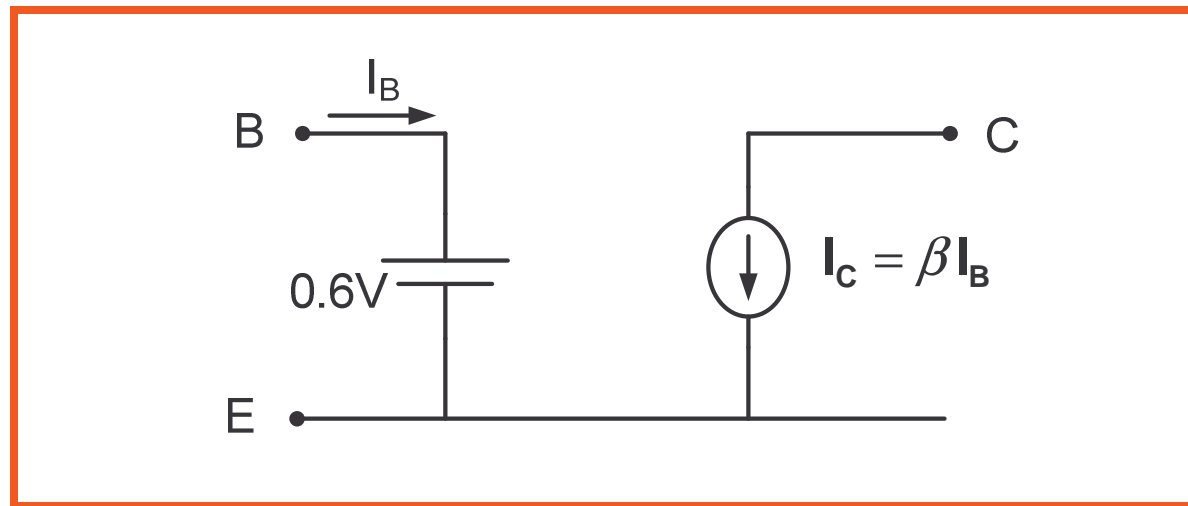


# Bipolar Models

## Simple dc Model for Biasing

$$V_{BE} = 0.6V$$

$$I_C = \beta I_B$$



When is this model justifiable ?

When it doesn't make much difference in the analysis of a circuit whether  $V_{BE} = 0.6V$  or  $0.7V$

When the VCE dependence on the collector current is negligible