EE 508 Lecture 44

Conventional Wisdom — Benefits and Consequences of Annealing Understanding of Engineering Principles

by Randy Geiger lowa State University

Summary of Recent Published Filter Architectures thanks to Yongjie Jiang

Summary by Application

I. Channel Selection Filter in communication system

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Applicati0on	Interests	Reference
GSM channel selection filter,	Low voltage design	2011, JSSC, pp.2268-
signal bandwidth: 100kHz		
WCDMA channel selection filter,	New (Active L) RC	2010,JSSC, pp.1770-
Signal bandwidth 2MHz	current biguads cell	
Channel selection and anti-aliasing	Using dominant poles of	2011,ISCAS,pp.1644
filter in receiver	opamps to create 4-th	
Cut-off frequency 11MHz	order filter in a single	
	cell	
Low IF Channel selection band-pass		2010,JSSC,pp.538
filter		
IF Central frequency 1MHz		
Channel selection filter for blue	Linearization skills	Garcia-Alberdi, 2012,
tooth and zigbee		TCAS1
cut off frequency 200kHz to 2Mhz		
Channel selection filter for zero IF		2012,TCASII,pp.30
and low IF receiver.		
IF frequency:		
4.1MHz to 20.6Mhz, Bandwidth:		
2.2 to 18MHz		
	GSM channel selection filter, signal bandwidth: 100kHz WCDMA channel selection filter, Signal bandwidth 2MHz Channel selection and anti-aliasing filter in receiver Cut-off frequency 11MHz Low IF Channel selection band-pass filter IF Central frequency 1MHz Channel selection filter for blue tooth and zigbee cut off frequency 200kHz to 2Mhz Channel selection filter for zero IF and low IF receiver. IF frequency: 4.1MHz to 20.6Mhz, Bandwidth:	GSM channel selection filter, signal bandwidth: 100kHz WCDMA channel selection filter, Signal bandwidth 2MHz Channel selection and anti-aliasing filter in receiver Cut-off frequency 11MHz Low IF Channel selection band-pass filter IF Central frequency 1MHz Channel selection filter for blue tooth and zigbee cut off frequency 200kHz to 2Mhz Channel selection filter for zero IF and low IF receiver. IF frequency: 4.1MHz to 20.6Mhz, Bandwidth:

II. RF Filters in communication system High frequency filter in receiver used as LO harmonic rejection, Sub-band filtering

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Architecture	Application	Interests	Reference
Passive RLC	RF filter, reject LO harmonics		2012,JSSC,pp.392
	LO frequency: 300Mhz to 800Mhz		
gm-C	RF Filter, reject LO harmonics	The author claims that	2012,JSSC,pp.1084
	LO frequency: 30Mhz to 900Mhz	linearity problem can be	
		relaxed due to	
		harmonic Rejection	
		Mixer	
Passive RLC	RF filter, reject LO harmonics	New method to select	2011 Electronics Letter
	filter sub-band noise in spectrum	passives.	November, No.24
	monitor receiver		
	Signal bandwidth 1G and 200MHz		
	LO frequency: 9.45G and 1.75G		
Passive RLC	reject LO harmonics		2010,TCASII,pp.522
	LO frequency: 24GHz		
Passive RC	Poly phase filter operate in 60GHz		2010,JSSC,pp.1644
	for sub-harmonic Mixers		
	-		

gm-C	Digital TV tuner	RF tracking technique	2011,Electronics Letter,
	LO frequency: 48MHz to 780MHz		pp.407
	bandwidth: 15MHz		
Hybrid RC-	Digital TV tuner,	Linearization skills	2011,TCASI,pp.2346
gm-C filter	LO frequency: 48Mhz to 200Mhz		
Switched	Digital TV tuner,		2011,JSSC,pp.998
resistor C	LO frequency:100MHz to 1GHz		
	bandwidth 35MHz		

III. Sub-audio frequency application

Architecture	Application	Interests	Reference
Active	5mHz cut off frequency for		2012, Electronics Letter,
MOSFET-C	electrophysiological		pp. 698
	signal acquisitions		
MOSFET-C	sub-Hz high-pass filter for sensors		2011,TCASI,pp.1561
MOSFET-C	Neural signal recording		2011,ISCAS,pp.1451
	HPF: 2.3Hz to 572Hz		
	LPF: 200Hz and 6.2kHz		

IV. Loop Filter In PLL

Architecture	Application	Interests	Reference
Switched	Loop Filter in PLL	Using Switched resistor	2011, JSSC, pp.2566-
resistor filter	PLL bandwidth 30KHz	filter to eliminate	
	PLL reference frequency 5MHz	charge pump and	
		reduce reference spur	
Switched	Used as loop filter in PLL with		2011,TCASII,pp.555
capacitor	reference frequency 10MHz for		
filter	reducing reference spur and		
	capacitor size		

V. Others

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<u> </u>			
Architecture	Application	Interests	Reference
R-MOSFET-C	91 to 268khz tuning range	Cross couple linear	2012,JSSC,pp.2751
		region transistor to	
		improve the linearity	
Active RC	7Mhz to 20Mhz cut-off frequency	Power efficient op-amp	2011,ISCAS,pp.2751
gm-C	100Hz to 10Mhz multiple purpose	Modified biquads	2011,TCASII.pp.159
	filter	structure to improve	
		the linearity	
gm-C	Motion Sensor	Floating gate array to	2011,ISCAS,pp.2425
		program cutoff	
		frequency	

MISO	10MHz Cut off frequency	Simple 7 transistors	2011,TCASII, pp.356
universal		new bi-quads cell for	
filter, 7		HP,LP and BP	
transistors		application	
biquad cell			
Digital Filter	Digital Hearing aids		2010,TCASI,pp.584

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Conventional Wisdom:

Conventional wisdom is the collective understanding of fundamental engineering concepts and principles that evolves over time through interactions of practicing engineers around the world

Conventional Wisdom:

- Guides engineers in daily practice of the Profession
- Widely use to enhance productivity
- Heavily emphasized in universities around the world when educating next-generation engineers
- Often <u>viewed</u> as a fundamental concept or principle
- Validity of conventional wisdom seldom questioned

Are Conventional Wisdom and Fundamental Concepts and Principles Always Aligned?



Much of Society till 1200AD to 1600AD and later

http://greenfunkdan.blogspot.com/2008/11/csiro-warns-of-climate-change-doomsday.html

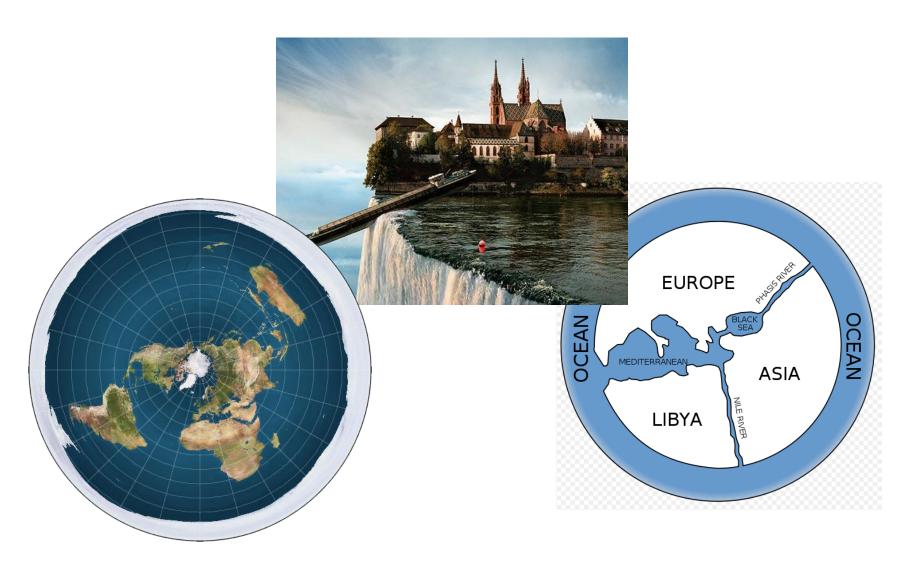


Pythagoras 520BC Aristotle 300BC

http://www.christiananswers.net/q-aig/aig-c034.html

Sometimes the differences can be rather significant!

Conventional wisdom, when not correctly representing fundamental principles, can provide conflicting perceptions or irresolvable paradoxes



Are Conventional Wisdom and Fundamental Concepts always aligned in the Microelectronics Field?



Introduction: This is "CW" who reflects the Conventional Wisdom that has evolved.



CW will share his views with us, on occasion, throughout this presentation

Are Conventional Wisdom and Fundamental Concepts always aligned in the Microelectronics Field?











Records of

- Conventional Wisdom
- Fundamental Concepts
- Occasional Oversight of Error
- Key information embedded in tremendous volume of materials (noise)

Conventional Wisdom

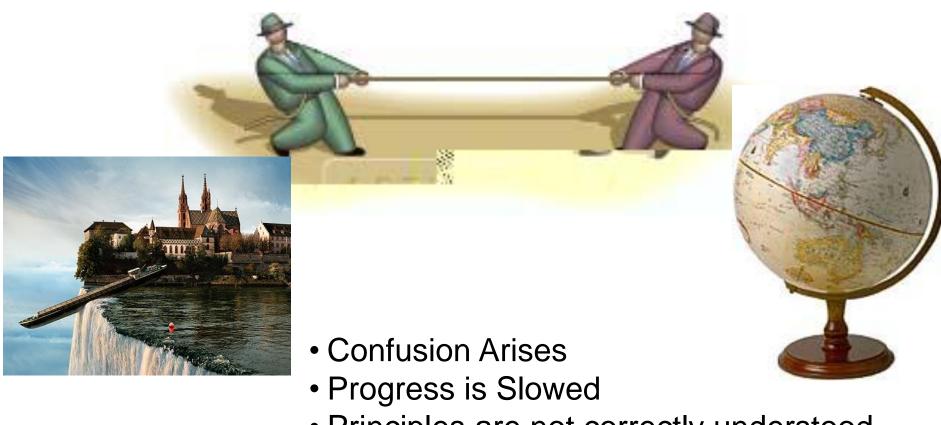
Do Conventional Wisdom and Fundamental Concepts Differ In the Microelectronics Field?



Reliability?

The process is good but not perfect!

What Happens When Fundamental Concepts and Conventional Wisdom Differ?



- Principles are not correctly understood
- Errors Occur
- Time is Wasted

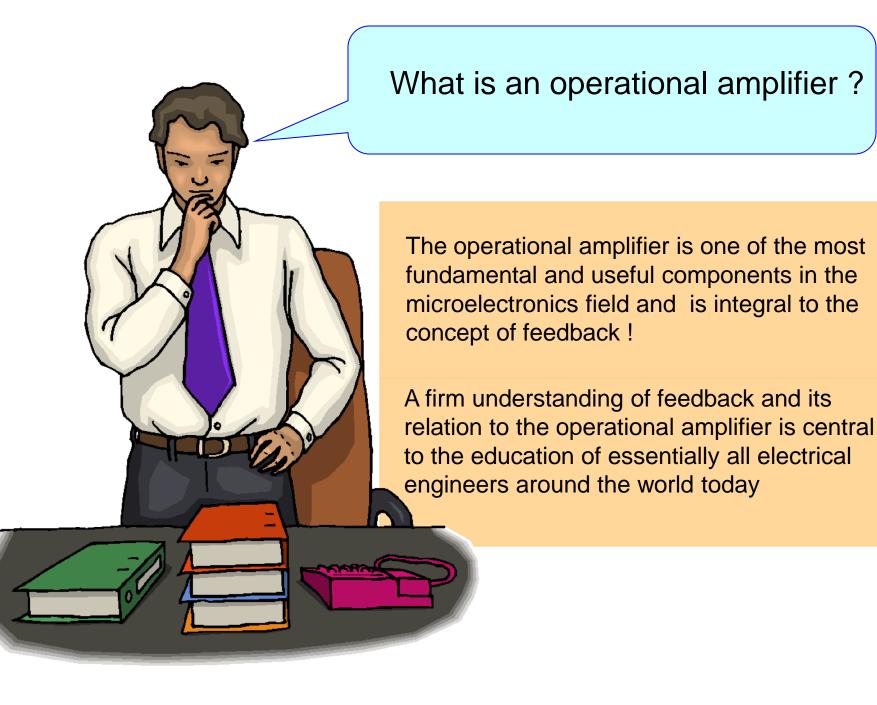
Are Conventional Wisdom and Fundamental Concepts always aligned in the Microelectronics Field?



Will consider 4 basic examples in this discussion



- Op Amp
 - Positive Feedback Compensation
 - Current Mode Filters
 - Current Dividers



What is an Operational Amplifier?

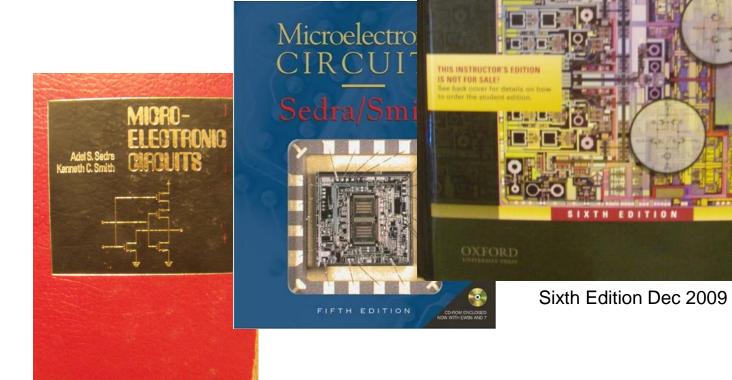
Lets see what the experts say!



Consider one of the most popular textbooks on the subject used in the world today

A classic textbook that has helped educate two

generations of engineers



SEDRA/SMITH

Microelectronic Circuits

First Edition 1982

In all editions, concept of the op amp has remained unchanged

2.1.2 Function and Characteristics of the Ideal Op Amp

We now consider the circuit function of the op amp. The op amp is designed to sense the difference between the voltage signals applied at its two input terminals (i.e., the quantity $v_2 - v_1$), multiply this by a number A, and cause the resulting voltage $A(v_2 - v_1)$ to appear at output terminal 3. Here it should be emphasized that when we talk about the voltage at a terminal we mean the voltage between that terminal and ground; thus v_1 means the voltage applied between terminal 1 and ground.

The ideal op amp is not supposed to draw any input current; that is, the signal current into terminal 1 and the signal current into terminal 2 are both zero. In other words, the input impedance of an ideal op amp is supposed to be infinite.

How about the output terminal 3? This terminal is supposed to act as the output terminal of an ideal voltage source. That is, the voltage between terminal 3 and ground will always be equal to $A(v_2 - v_1)$, independent of the current that may be drawn from terminal 3 into a load impedance. In other words, the output impedance of an ideal op amp is supposed to be zero.

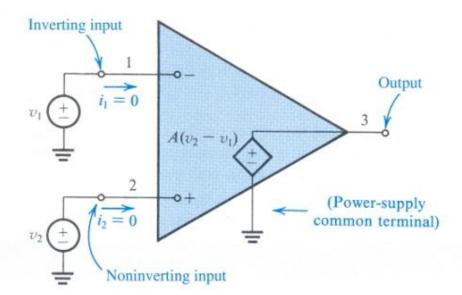
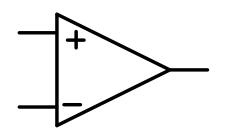


FIGURE 2.3 Equivalent circuit of the ideal op amp.

TABLE 2.1 Characteristics of the Ideal Op Amp

- 1. Infinite input impedance
- 2. Zero output impedance
- 3. Zero common-mode gain or, equivalently, infinite common-mode rejection
- 4. Infinite open-loop gain A
- 5. Infinite bandwidth

What is an Operational Amplifier?



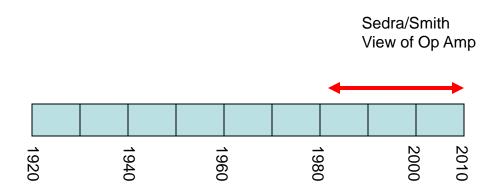
Textbook Definition:

- Voltage Amplifier with Very Large Gain
 - -Very High Input Impedance
 - -Very Low Output Impedance
- Differential Input and Single-Ended Output

This represents the Conventional Wisdom!

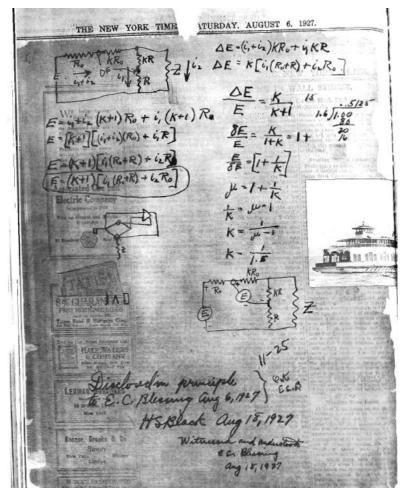
Does this correctly reflect what an operational amplifier really is?

Operational Amplifier Evolution in Time Perspective



Consider some history leading up to the present concept of the

operational amplifier



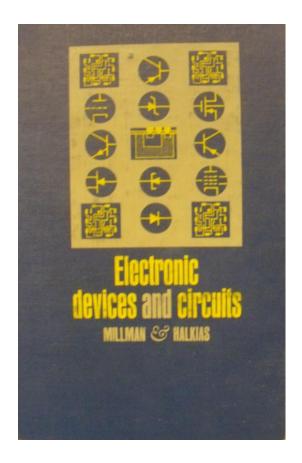
H.S. Black sketch of basic concept of feedback on Aug 6, 1927

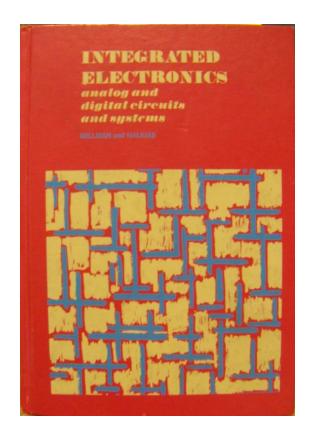
Black did not use the term operational amplifier but rather focused on basic concepts of feedback involving the use of high-gain amplifiers

A classic textbook sequence that has helped educate the previous two generations of engineers

Vacuum Tube and Semiconductor Electronics

By Millman



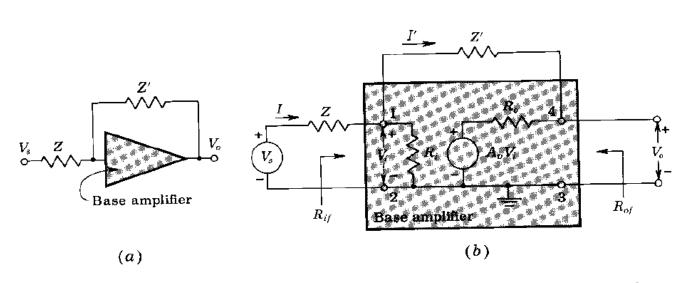


First Edition 1958

First Edition 1967

First Edition 1972

Millman view of an operational amplifier in 1967



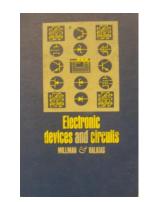


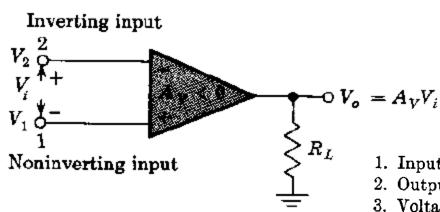
Fig. 17-26 (a) Schematic diagram and (b) equivalent circuit of an operational amplifier. The open-circuit voltage gain $A_{\it v}$ is negative.

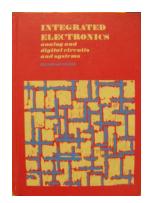
Operational Amplifier refers to the entire feedback circuit

Concept of a "Base Amplifier" as the high-gain amplifier block

Note Base Amplifier is modeled as a voltage amplifier with single-ended input and output

Millman view of an operational amplifier in 1972





- 1. Input resistance $R_i = \infty$
- 2. Output resistance $R_o = 0$
- 3. Voltage gain $A_v = -\infty$
- 4. Bandwidth = ∞
- 5. $V_0 = 0$ when $V_1 = V_2$ independent of the magnitude of V_1
- 6. Characteristics do not drift with temperature.

This book was published several years after the first integrated op amps were introduced by industry

This fundamentally agrees with that in use today by most authors

Major change in the concept from his own earlier works

Seminal source for "Operational Amplifier" notation:

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PROCEEDINGS OF THE I.R.E.

May 1947

Analysis of Problems in Dynamics by Electronic Circuits*

JOHN R. RAGAZZINI[†], MEMBER, I.R.E., ROBERT H. RANDALL[‡], AND FREDERICK A. RUSSELL[§], MEMBER, I.R.E.

The term "operational amplifier" is a generic term applied to amplifiers whose gain functions are such as to enable them to perform certain useful operations such as summation, integration, differentiation, or a combination of such operations.

Seminal source introduced a fundamentally different definition than what is used today

Consistent with the earlier use of the term by Millman

Seminal Publication of Feedback Concepts:

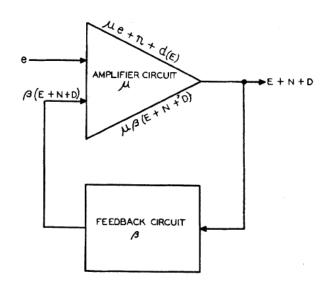
Stabilized Feed-Back Amplifiers

By H. S. BLACK MEMBER A.I.E.E.

Bell Telephone Laboratories, Inc., New York, N. Y.

Transactions of the American Institute of Electrical Engineers, Jan. 1934

Fig. 1. Amplifier system with feed-back

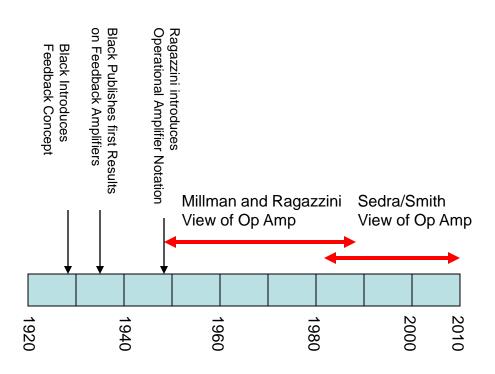


Uses a differential input high-gain voltage amplifier (voltage series feedback)

Subsequent examples of feedback by Black relaxed the differential input requirement

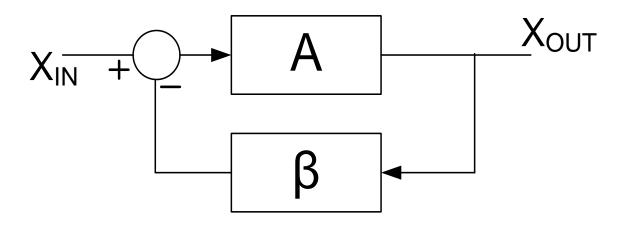
APCAS 2010

Operational Amplifier Evolution in Time Perspective



Do we have it right now?

Why are Operational Amplifiers Used?

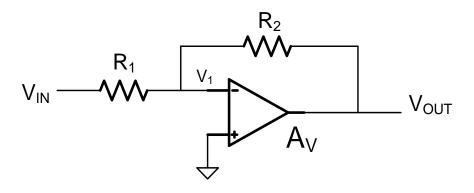


Input and Output Variables intentionally designated as "X" instead of "V"

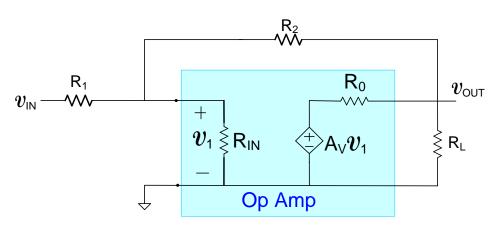
$$\frac{\text{Xout}}{\text{Xin}} = A_F = \frac{A}{1 + A\beta} = \overset{A \to \infty}{\approx} \frac{1}{\beta}$$

Op Amp is Enabling Element Used to Build Feedback Networks!

One of the Most Basic Op Amp Applications



Model of Op Amp/Amplifier including A_V, R_{IN}, R_O and R_L

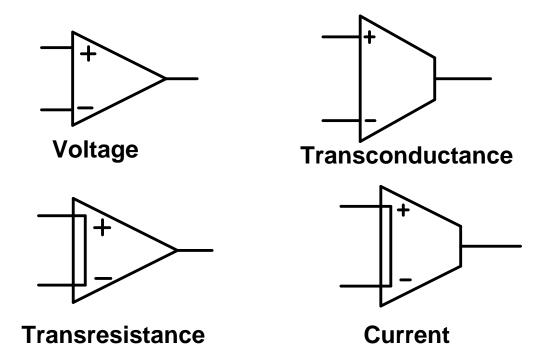


If it is assumed that A_{V} is large,

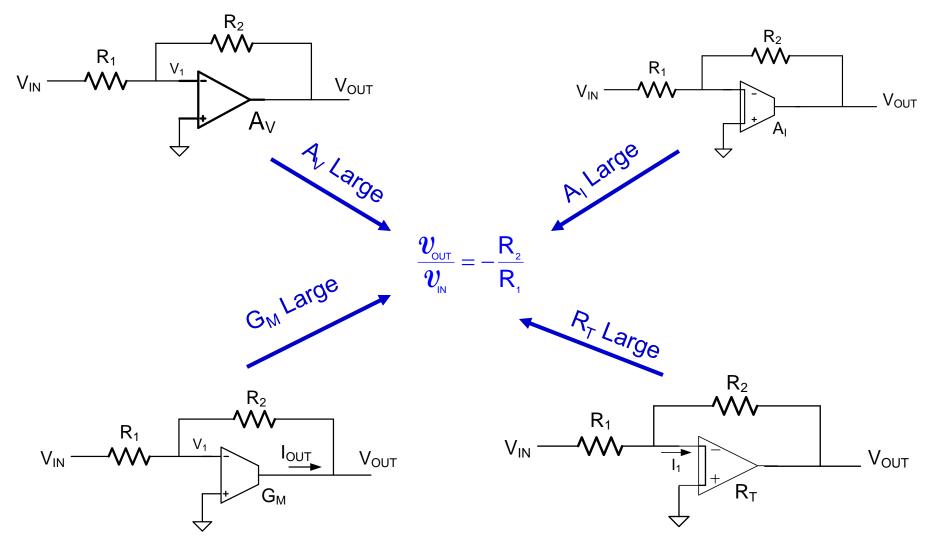
$$\mathsf{A}_{\scriptscriptstyle\mathsf{VF}} = rac{oldsymbol{v}_{\scriptscriptstyle\mathsf{OUT}}}{oldsymbol{v}_{\scriptscriptstyle\mathsf{N}}} \simeq -rac{\mathsf{R}_{\scriptscriptstyle\mathsf{2}}}{\mathsf{R}_{\scriptscriptstyle\mathsf{4}}}$$

This result is not dependent upon R_{IN} , R_0 or R_1

The Four Basic Types of Amplifiers:



Four Feedback Circuits with Same β Network

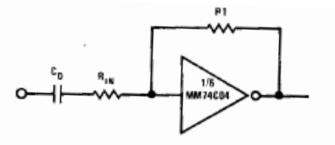


All have same closed-loop gain and all are independent of R_{IN}, R_{OUT} and R_L if gain is large

Concept well known

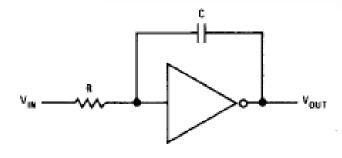


AN-88 CMOS LINEAR APPLICATIONS



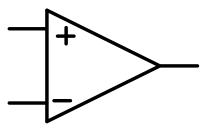
Bene Taatjes JULY 1973

FIGURE 2. A 74CMOS Invertor Biased for Linear Mode Operation.



Integrator Using
Any Inverting CMOS Gate

What is an Operational Amplifier?



Textbook Definition:

- Voltage Amplifier with Very Large Gain
 - -Very High Input Impedance
 - -Very Low Output Impedance

This represents the Conventional Wisdom!

Do we have it right now?

Voltage Amplifier?

Low Output Impedance?

Single-Ended Output?

High Input Impedance?

Differential Input?

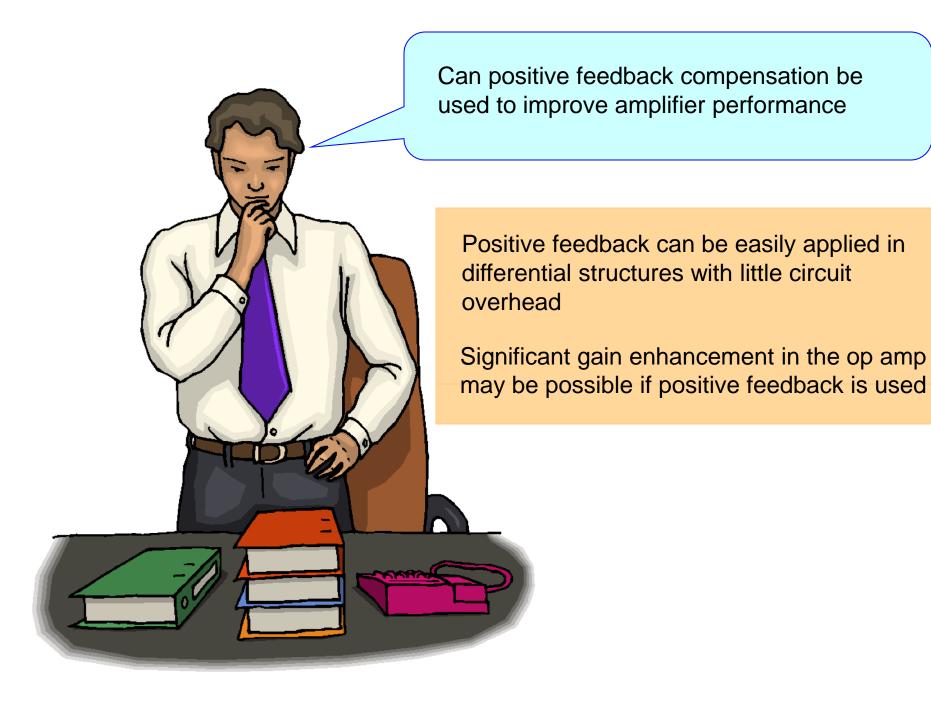
Large Gain !!!

Are Conventional Wisdom and Fundamental Concepts always aligned in the Microelectronics Field?



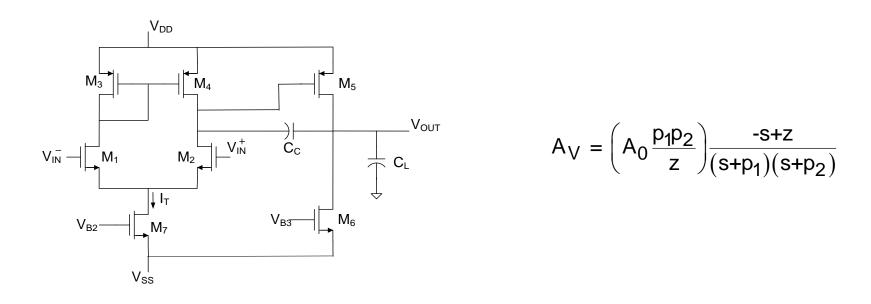
Will consider 4 basic examples in this discussion

- Op Amp
- Positive Feedback Compensation
 - Current Mode Filters
 - Current Dividers



Compensation of two-stage amplifiers

To illustrate concept consider basic two-stage op amp with internal compensation

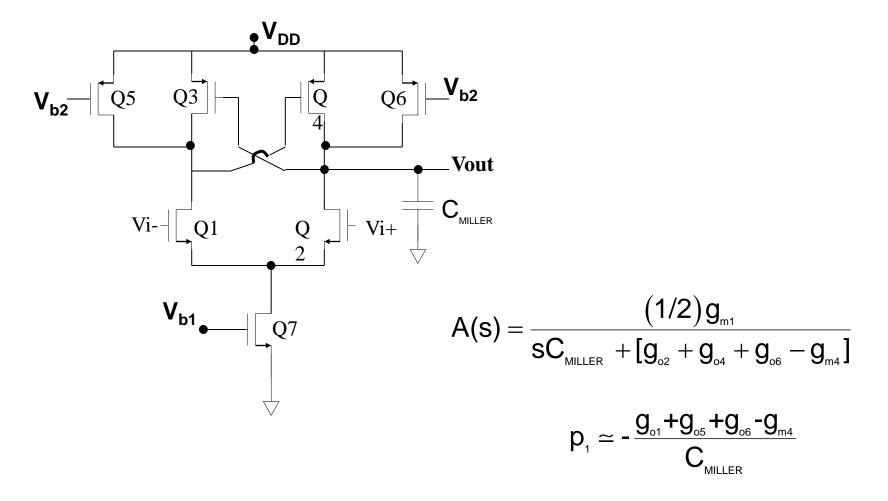


Miller Effect on C_C provides dominant pole on first stage Compensation requires a large ratio of p₂/p₁ be established

Two-stage amplifier with LHP Zero Compensation

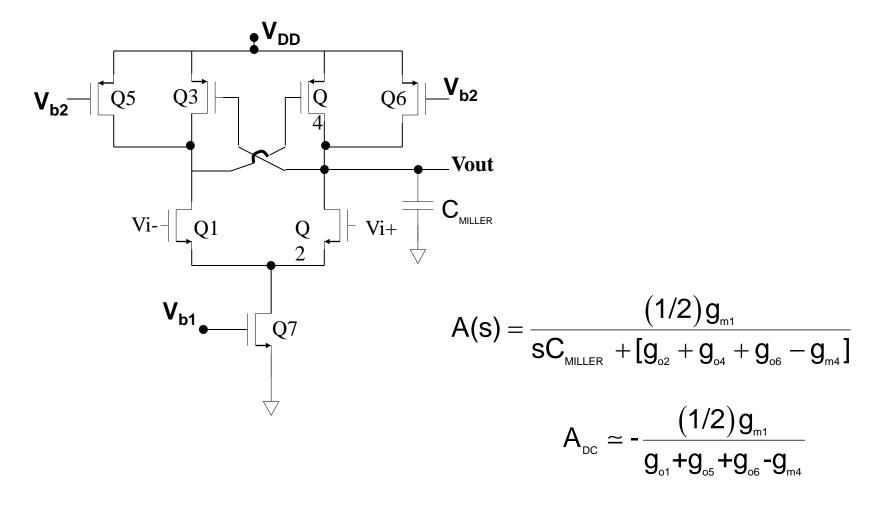
To make p₁ sufficiently dominant requires a large value for C_C

Positive Feedback on First-Stage for gain enhancement and pole control



Can reduce size of C_{MILLER} and enhance dc gain by appropriate choice of g_{m4} Can actually move p_1 into RHP if g_{m4} is too big

Positive Feedback on First-Stage for gain enhancement and pole control



Dc gain actually goes to ∞ when $g_{m1} = g_{02} + g_{04} + g_{06}$!

This technique is not practical since Op Amp pole can move into RHP making it unstable!

$$p_{_1} \simeq -\frac{g_{_{o1}} + g_{_{o5}} + g_{_{o6}} - g_{_{m4}}}{C_{_{MILLER}}}$$

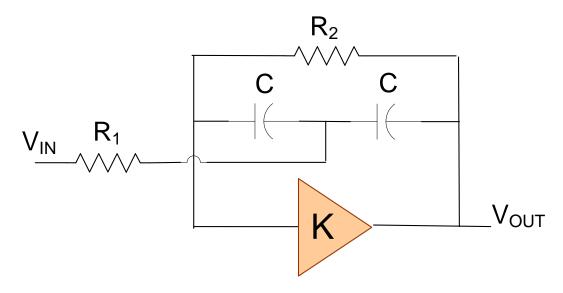


Several authors have discussed this approach in the literature but place a major emphasis on limiting the amount of positive feedback used so that under PVT variations, op amp remains stable



Example: Filter Structure with Feedback Amplifier

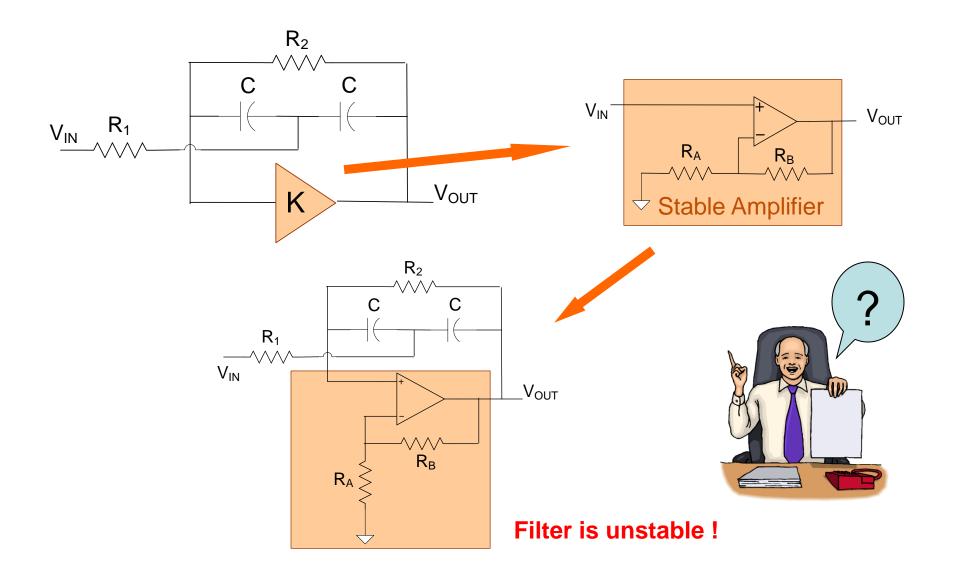
Bridged-T Feedback (Termed SAB, STAR, Friend/Delyannis Biquad)



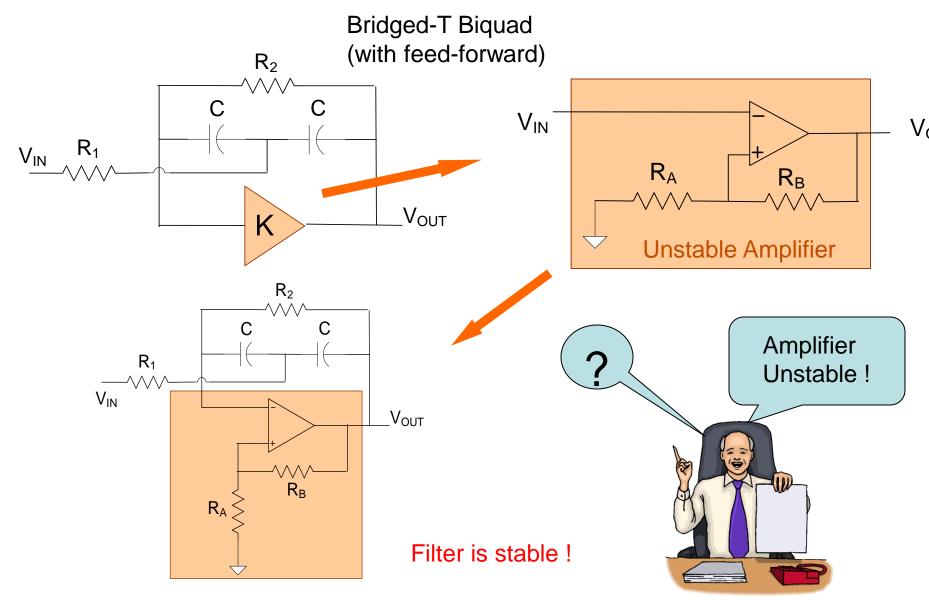
K is a small positive gain want high input impedance on "K" amplifier

- Very popular filter structure
- One of the best 2nd-order BP filters
- Widely used by Bell System in 70's

Example: Filter Structure with Feedback Amplifier



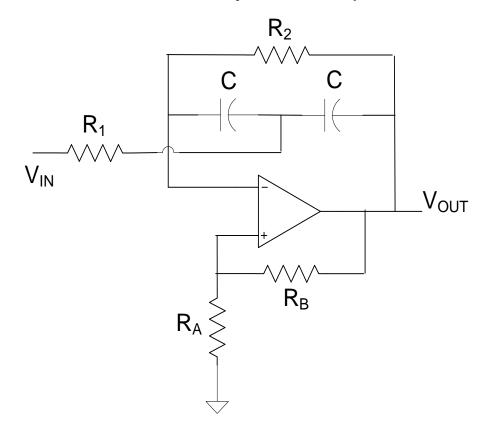
Example: Filter Structure with Feedback Amplifier



Friend/Deliyannis Biquad

Very Popular Bandpass Filter

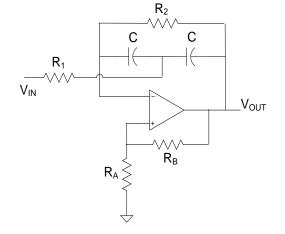
Friend-Deliyannis Biquad



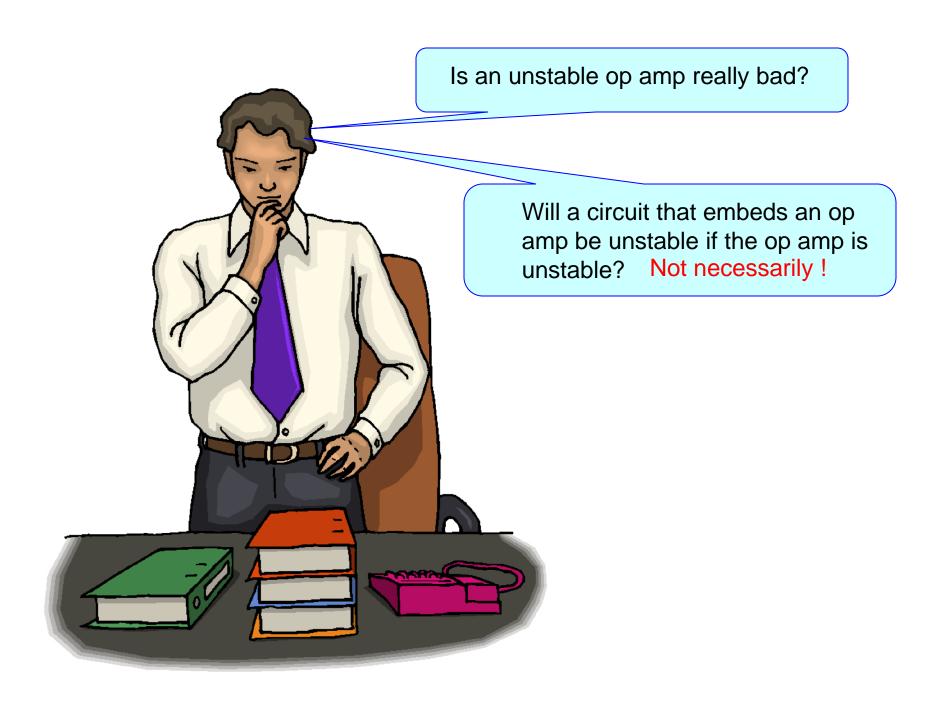
One of the best bandpass filters !!

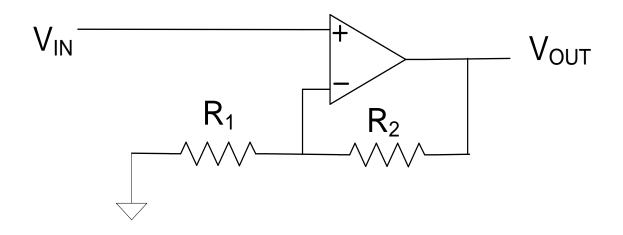
Embedded finite gain amplifier is unstable!!

Stability of embedded amplifier is not necessary (or even desired)

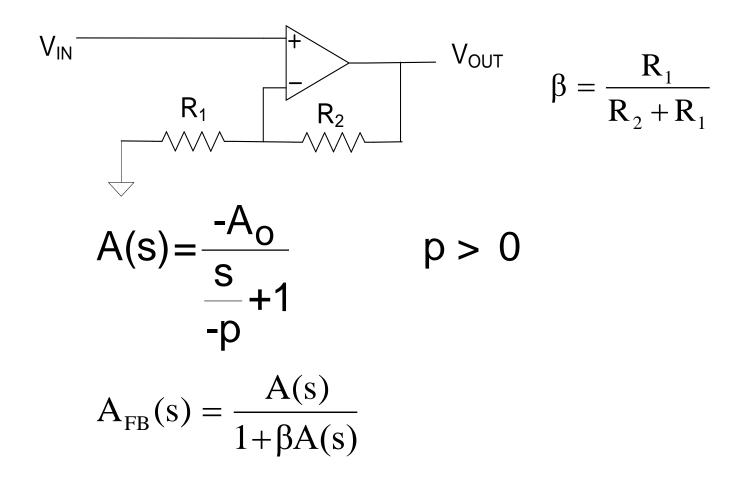


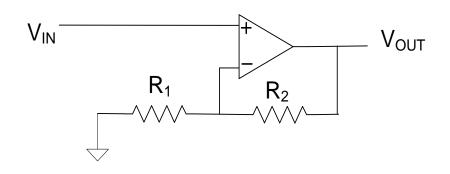
- Filter structure unstable with stable finite gain amplifier
- Filter structure stable with unstable finite gain amplifier
- Stability of feedback network not determined by stability of amplifier!





$$A(s) = \frac{-A_0}{\frac{s}{-p} + 1}$$
 p > 0

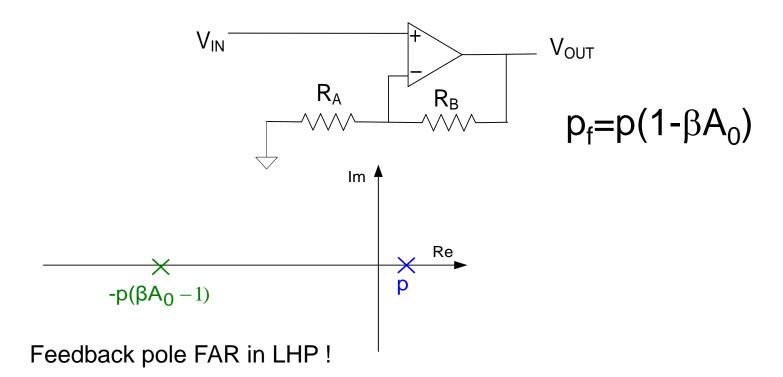




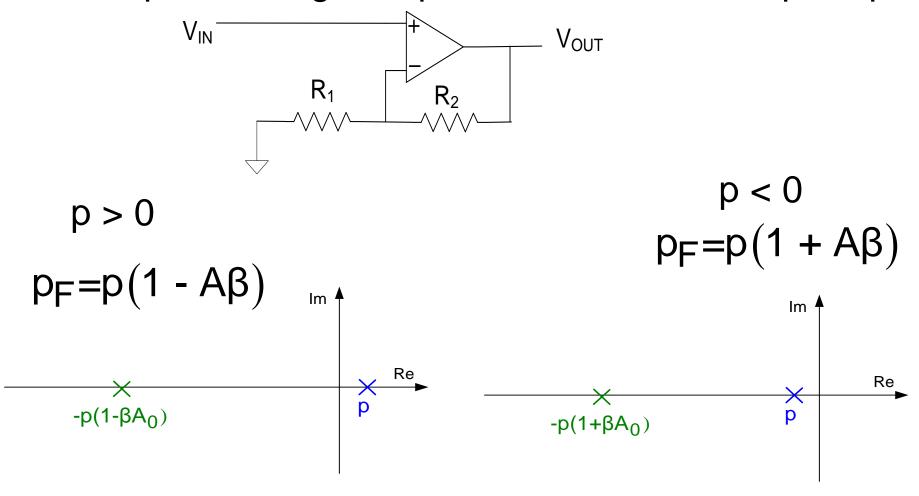
$$A_{FB}(s) = \frac{A(s)}{1+\beta A(s)} = \frac{A_{O}p}{s+p(\beta A_{O}-1)}$$
 $p > 0$

$$p_f = p(1-\beta A_0)$$

For $\beta A_0 > 1$, Feedback Amplifier is Stable !!!



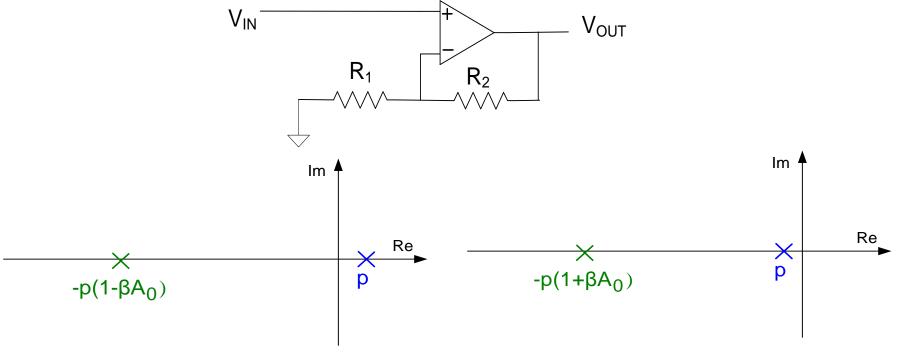
How does this compare to the feedback pole of a stable op amp with a pole In the LHP at –p?



Feedback pole FAR in LHP!

Feedback pole FAR in LHP!

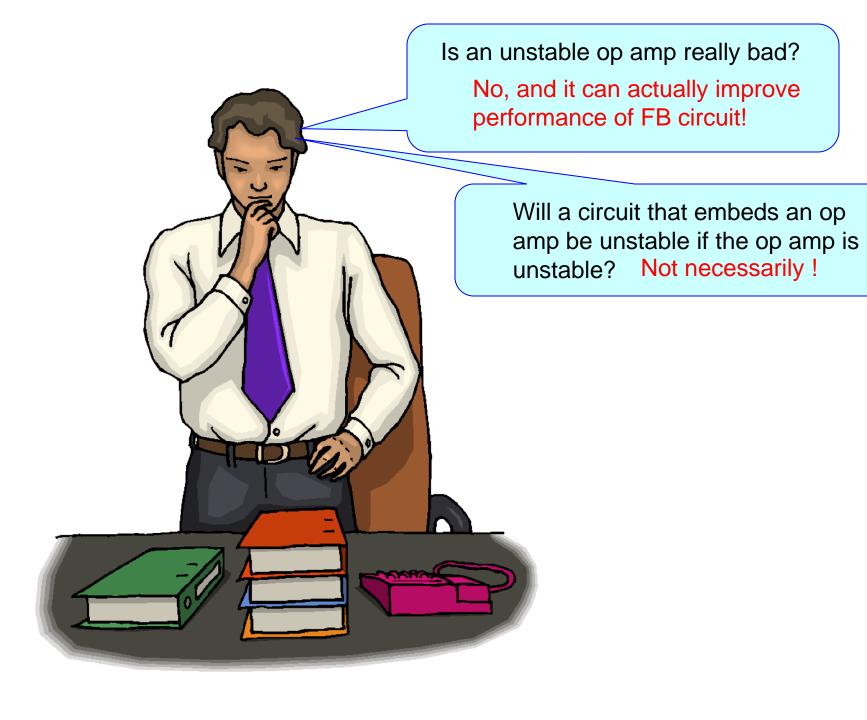
Can show that some improvements in feedback performance can be realized if the open-loop pole is at the orgin or modestly in the RHP!



Stability of open-loop amplifier is not a factor in determining the stability of the feedback structure in practical structures when |p| is small!

It can actually be shown that the performance of the feedback amplifier can be improved if the open-loop pole is moved modestly into the RHP

This is contrary to the Conventional Wisdom!

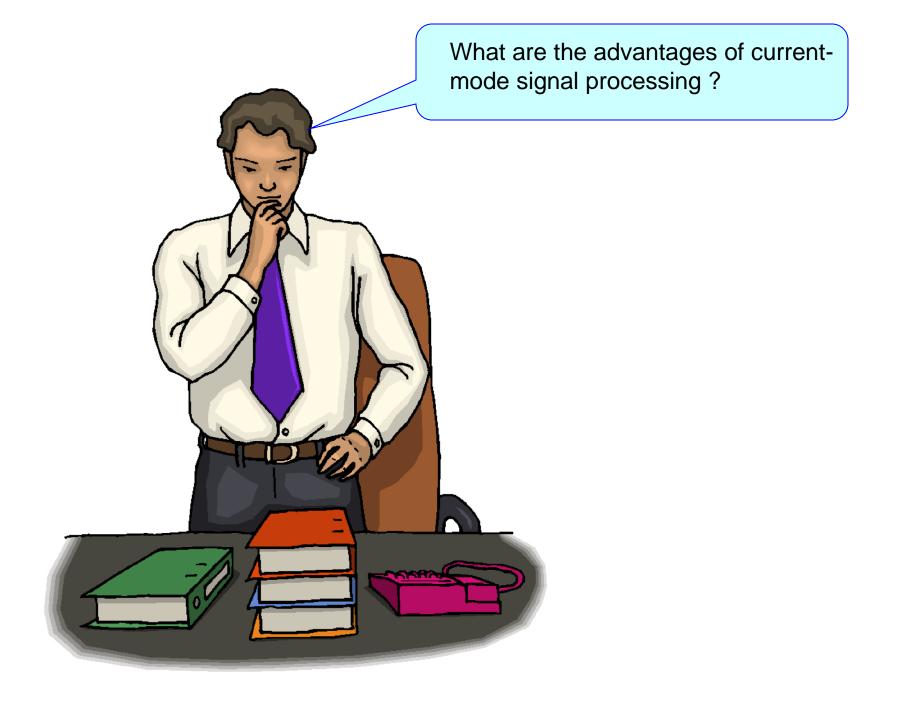


Are Conventional Wisdom and Fundamental Concepts always aligned in the Microelectronics Field?



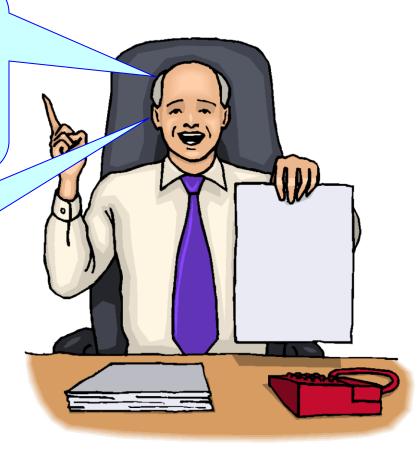
Will consider 4 basic examples in this discussion

- Op Amp
- Positive Feedback Compensation
- Current Mode Filters
- Current Dividers



EVERYBODY knows that Current-Mode circuits operate at lower supply voltages, are faster, are smaller, consume less power, and take less area than their voltage-mode counterparts!

And I've heard there are even some more benefits but with all of these, who really cares?



Have considered Current Mode Filters in Lecture 31 and 32

Showed by example that an Active RC Current-Mode Filter was identical to a Voltage-Mode Counterpart

Will now look at more general Current-Mode Architectures



- Why does a current-mode circuit work better at high frequencies?
- Why is a current-mode circuit better suited for low frequencies?
- Why do some "voltage"-mode circuits have specs that are as good as the current-mode circuits?

- Why are most of the papers on current-mode circuits coming from academia?
- Why haven't current-mode circuits replaced "voltage"-mode circuits in industrial applications?

What is a current-mode circuit?

- Everybody seems to know what it is
- Few have tried to define it
- Is a current-mode circuit not a voltagemode circuit?

What is a current-mode circuit?

"Several analog CMOS continuous-time filters for high frequency applications have been reported in the literature... Most of these filters were designed to process voltage signals. It results in high voltage power supply and large power dissipation. To overcome these drawbacks of the voltage-mode filters, the current-mode filters circuits, which process current signals have been developed"

A 3V-50MHz Analog CMOS Current-Mode High Frequency Filter with a Negative Resistance Load, pp. 260...,IEEE Great Lakes Symposium March 1996.

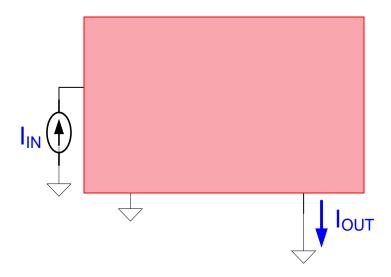
- Are current-mode circuits really better than their "voltage-mode" counterparts?
- What is a current-mode circuit?
 - Must have a simple answer since so many authors use the term
- Do all agree on the definition of a current-mode circuit?

Questions about the Conventional Wisdom Conventional Wisdom Definition:

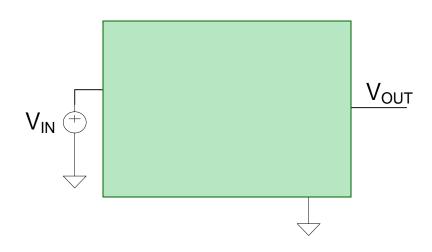
- A current-mode circuit is a circuit that processes current signals
- A current-mode circuit is one in which the defined state variables are currents

Example:

Is this a current-mode circuit?



Is this a voltage-mode circuit?



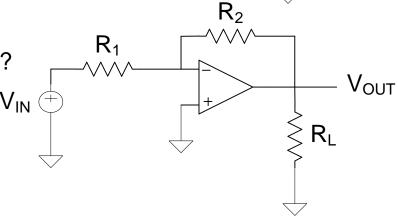
Conventional Wisdom Definition:

A current-mode circuit is a circuit that processes current signals

Example:

Is this a current-mode circuit?

Is this a voltage-mode circuit?



- One is obtained from the other by a Norton to Thevenin Transformation
- The poles and the BW of the two circuits are identical!

Current-Mode Filters

Concept of Current-Mode Filters is Somewhat Recent:

Key paper that generated interest in current-mode filters (ISCAS 1989):

Switched currents-a new technique for analog sampled-data signal processing

JB Hughes, NC Bird... - Circuits and Systems, 1989 ..., 2002 - ieeexplore.ieee.org NTRODUCTION The enormous complexity available in state-of-the-art CMOS processing has made possible the integration of complete systems, including both digital and analog signal processing functions, within the same chip Through the last decade, the **switched** capacitor technique $oldsymbol{...}$

Cited by 151 - Related articles

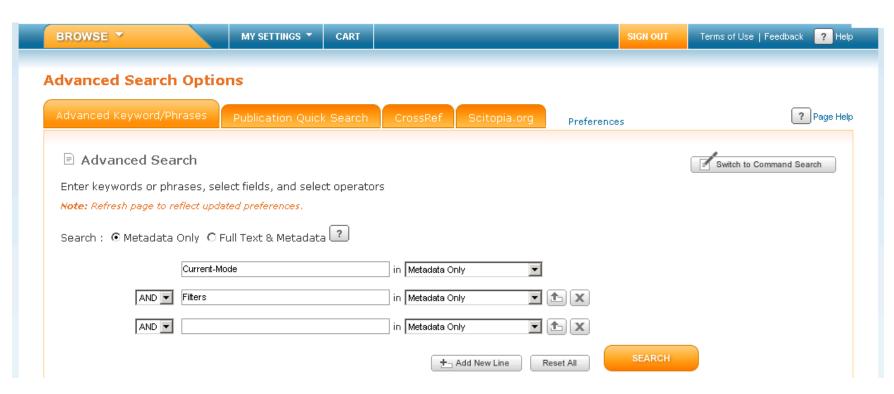
This paper is one of the most significant contributions that has ever come from ISCAS

Current-Mode Filters

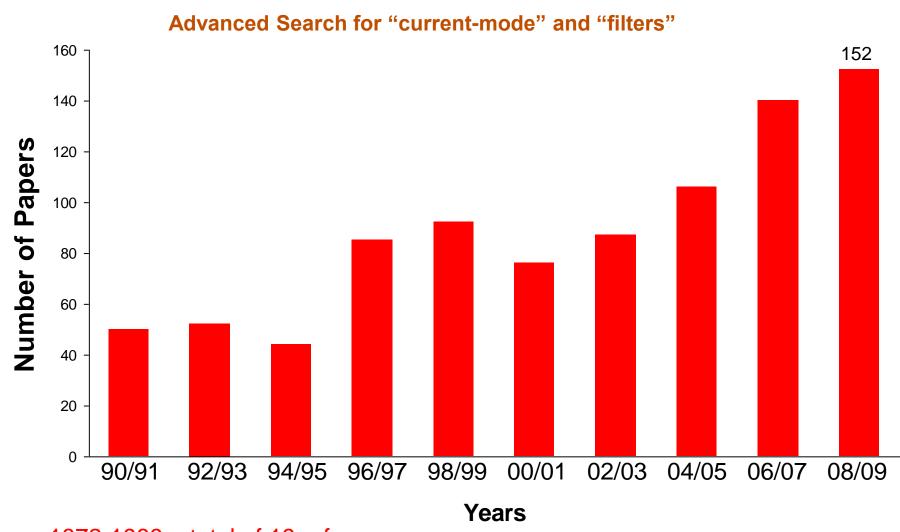


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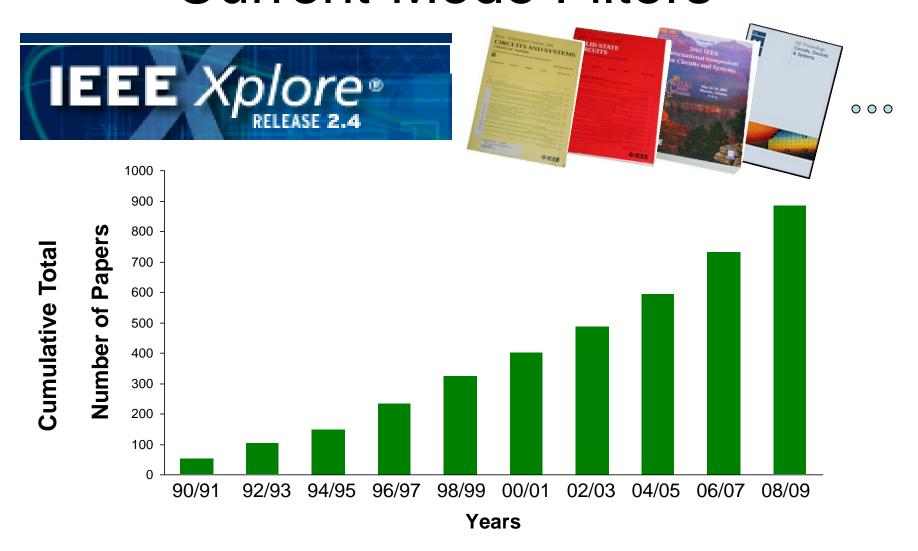




Current-Mode Filters



Review from Earlier Lecture Current-Mode Filters



Steady growth in research in the area since 1990 and publication rate is growing with time!!

The Conventional Wisdom:

Proc. ICASP May 2010:



It is well known that current-mode circuits can offer many advantages, such as simplicity of circuit structure, high-frequency operation, wide dynamic range, and so on, compared with their voltage-mode counterparts.



IEEE Trans. On Consumer Electronics, Feb 2009

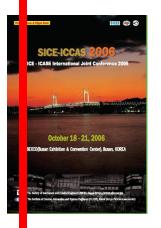
Current mode signal processing is a better solution than conventional voltage mode processing for high speed, low power and low voltage analog circuit design.

The Conventional Wisdom:



Proc. IEE Dec 2006:

Current-mode circuits have been proven to offer advantages over their voltage-mode counterparts [1, 2]. They possess wider bandwidth, greater linearity and wider dynamic range. Since the dynamic range of the analogue circuits using low-voltage power supplies will be low, this problem can be solved by employing current-mode operation.



Proc. SICE-ICASE, Oct. 2006

It is well known that current-mode circuits have been receiving significant attention owing to its advantage over the voltage-mode counterpart, particularly for higher frequency of operation and simpler filtering structure [1].

The Conventional Wisdom:



JSC April 1998:

"... current-mode functions exhibit higher frequency potential, simpler architectures, and lower supply voltage capabilities than their voltage-mode counterparts."



CAS June 1992

"Current-mode signal processing is a very attractive approach due to the simplicity in implementing operations such as ... and the potential to operate at higher signal bandwidths than their voltage mode analogues" ... "Some voltage-mode filter architectures using transconductance amplifiers and capacitors (TAC) have the drawback that ..."

The Conventional Wisdom:

ISCAS 1993:



"In this paper we propose a fully balanced high frequency current-mode integrator for low voltage high frequency filters. Our use of the term current mode comes from the use of current amplifiers as the basic building block for signal processing circuits. This fully differential integrator offers significant improvement even over recently introduced circuit with respect to accuracy, high frequency response, linearity and power supply requirements. Furthermore, it is well suited to standard digital based CMOS processes."

The Conventional Wisdom:

Two key publications where benefits of the current-mode circuits are often referenced:



All current-mode frequency selective circuits GW Roberts, AS Sedra - Electronics Letters, June 1989 - pp. 759-761 Cited by 228

"To make greatest use of the available transistor bandwidth f_T , and operate at low voltage supply levels, it has become apparent that analogue signal processing can greatly benefit from processing current signals rather than voltage signals. Besides this, it is well known by electronic circuit designers that the mathematical operations of adding, subtracting or multiplying signals represented by currents are simpler to perform than when they are represented by voltages. This also means that the resulting circuits are simpler and require less silicon area."

The Conventional Wisdom:

Two key publications where benefits of the current-mode circuits are often referenced:



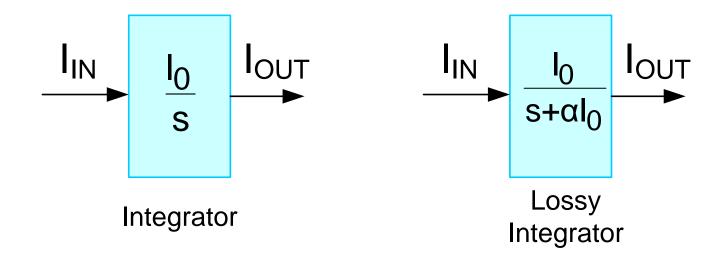
Recent developments in current conveyors and current-mode circuits B Wilson - Circuits, Devices and Systems, IEE Proceedings G, pp. 63-77, Apr. 1990 Cited by 288

"The **use** of current rather than voltage as the active parameter can result in higher usable gain, accuracy and bandwidth due to reduced voltage excursion at sensitive nodes. A current-mode approach is not just restricted to current processing, but also offers certain important advantages when interfaced to voltage-mode circuits."

The Conventional Wisdom:

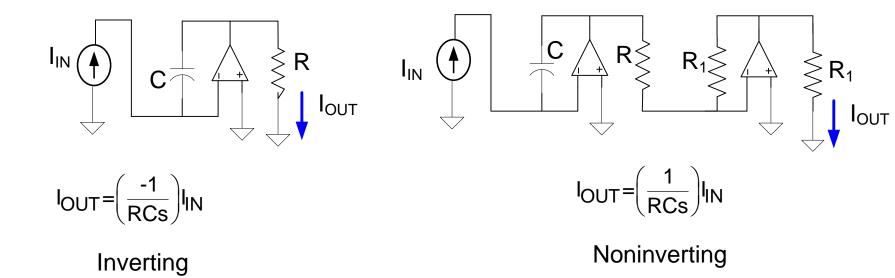
- Current-Mode circuits operate at higherfrequencies than voltage-mode counterparts
- Current-Mode circuits operate at lower supply voltages and lower power levels than voltagemode counterparts
- Current-Mode circuits are simpler than voltage-mode counterparts
- Current-Mode circuits offer better linearity than voltage-mode counterparts

This represents four really significant benefits of current-mode circuits!



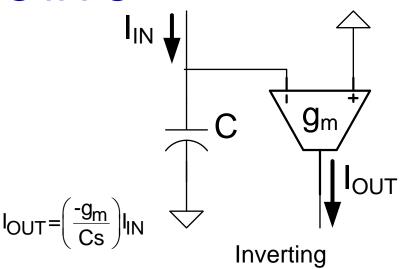
As with voltage-mode filters, most integrated currentmode filters are built with integrators and lossy integrators

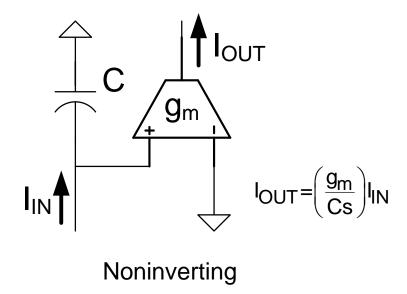
Active RC



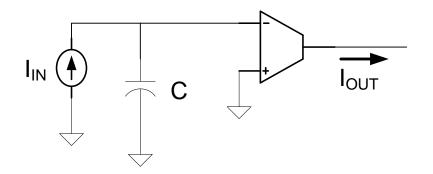
- Summing inputs really easy to obtain
- Loss is easy to add
- Some argue that since only interested in currents, can operate at lower voltages

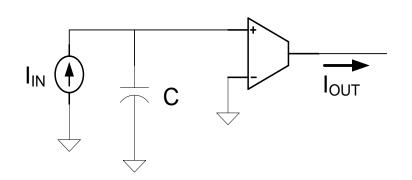
OTA-C

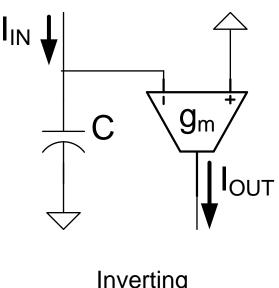


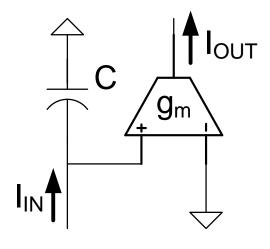


Alternate representation





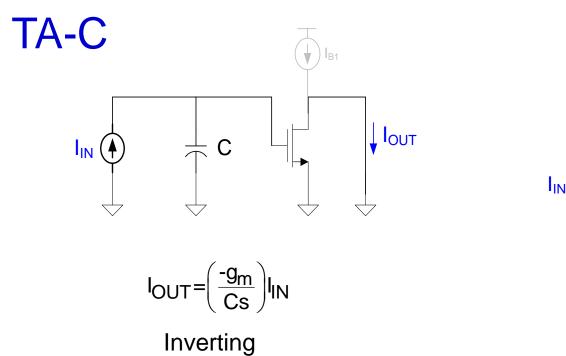


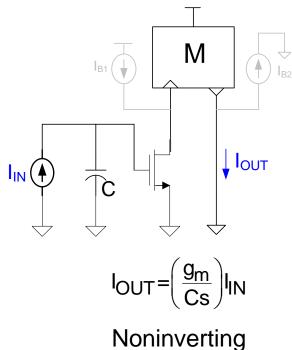


Inverting

Noninverting

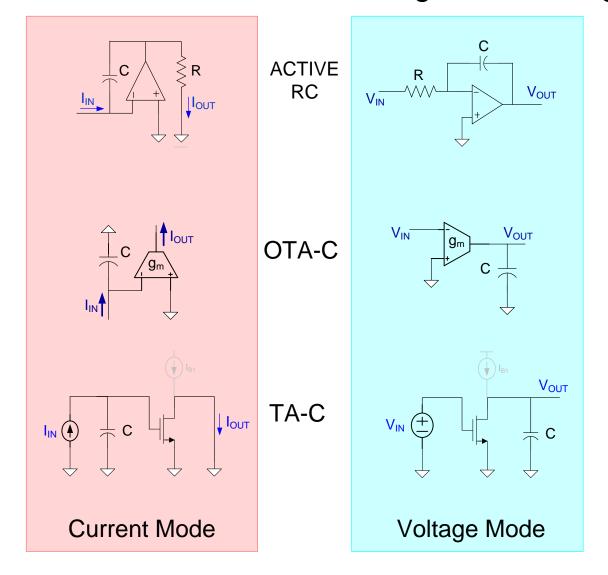
- Summing inputs really easy to obtain
- Loss is easy to add
- Many argue that since only interested in currents, can operate at lower voltages and higher frequencies





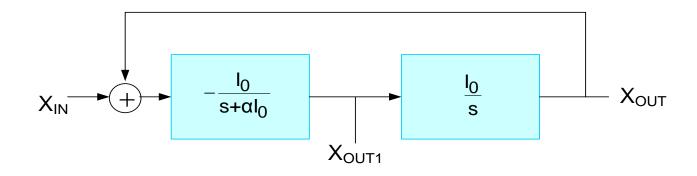
- Summing inputs really easy to obtain
- Loss is easy to add
- Many argue that since only interested in currents, can operate at lower voltages and higher frequencies

Comparison of Current Mode and Voltage Mode Integrators



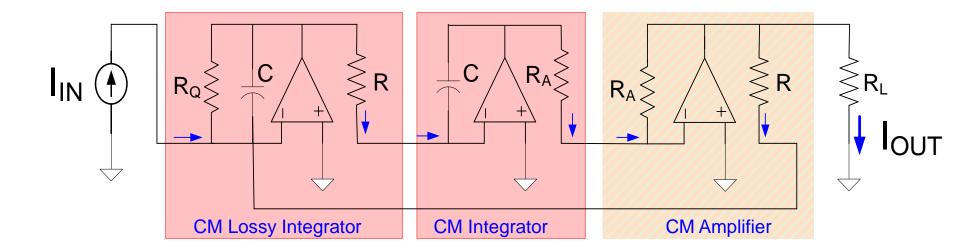
- Current Mode and Voltage Mode Inverting integrators have same device counts
- Same is true of noninverting and lossy structures

Review from Earlier Lecture Two-Integrator-Loop Biquad



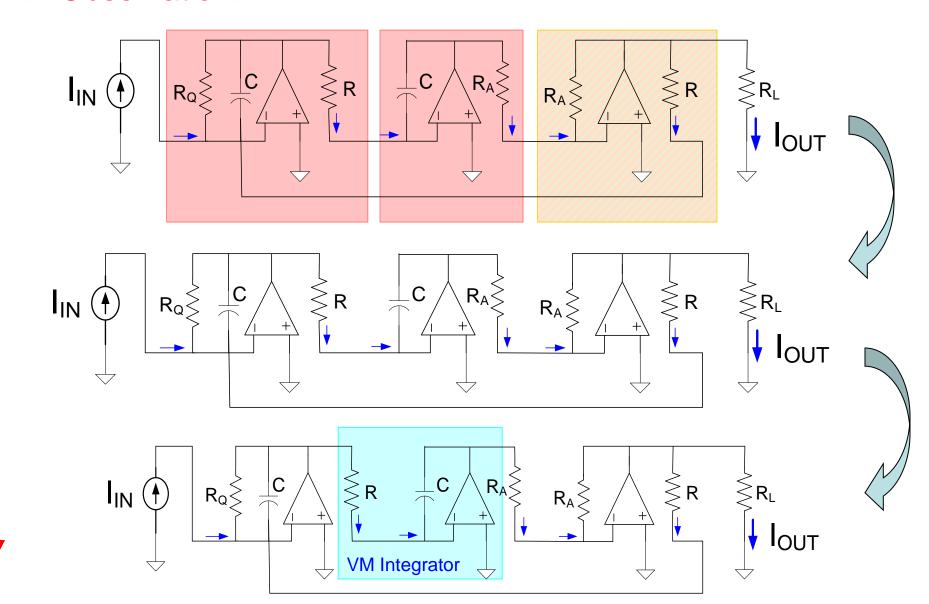
One of the most widely used architectures for implementing integrated filters

Active RC Current-Mode implementation

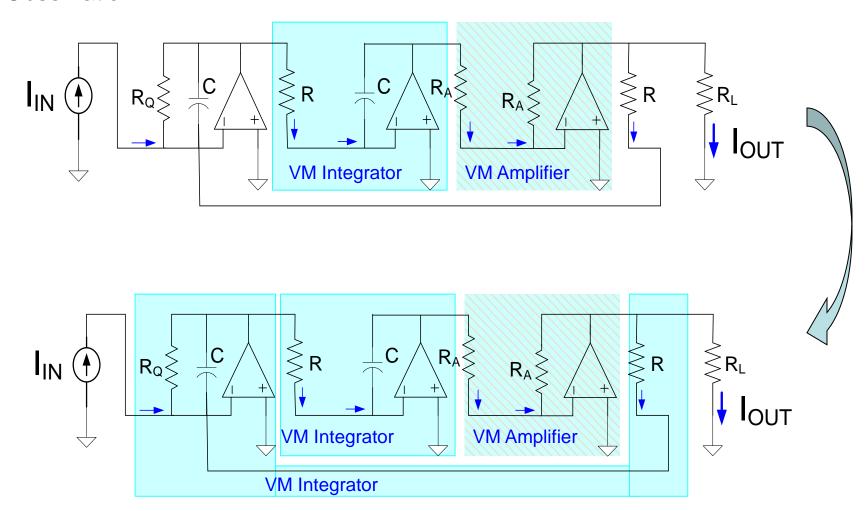


- Straightforward implementation of the two-integrator loop
- Simple structure

An Observation:



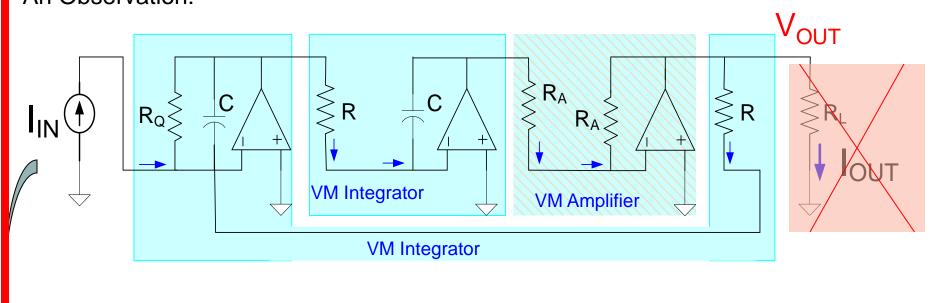
An Observation:

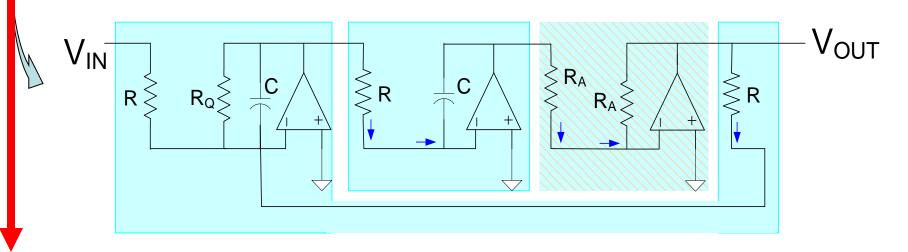


This circuit is identical to another one with two voltage-mode integrators and a voltage-mode amplifier!

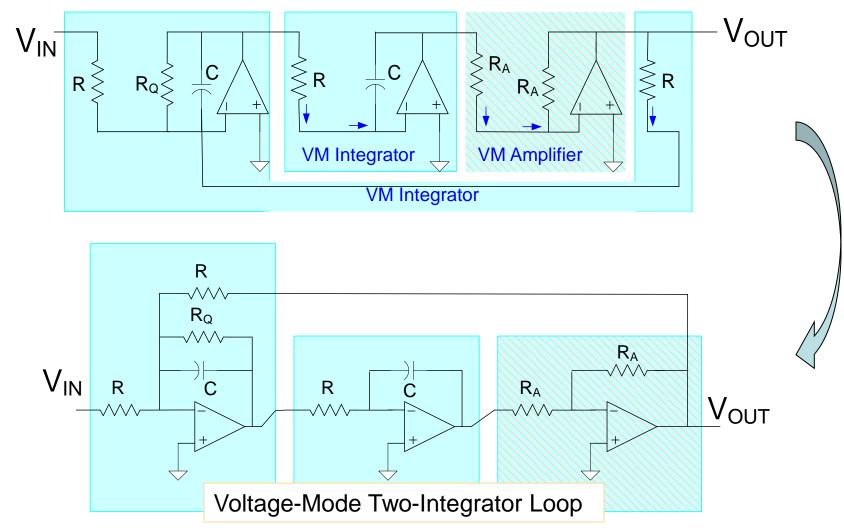
An Observation: V_{OUT} R_Q VM Integrator **VM** Amplifier **VM Integrator** I_{IN}

An Observation:





An Observation:

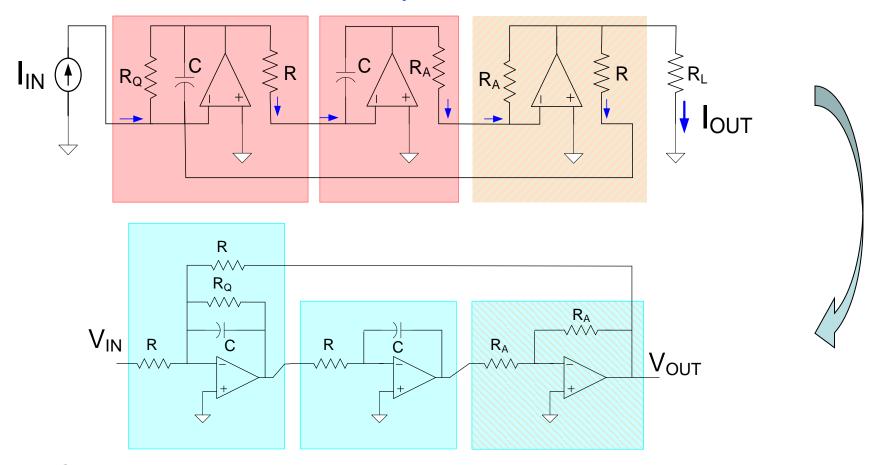


This circuit was well-known in the 60's

Review from Earlier Lecture

Current-Mode Two Integrator Loop

Active RC Current-Mode implementation



Current-mode and voltage-mode circuits have same component count Current-mode and voltage-mode circuits are identical!

Current-mode and voltage-mode properties are identical!

Current-mode circuit offers NO benefits over voltage-mode counterpart

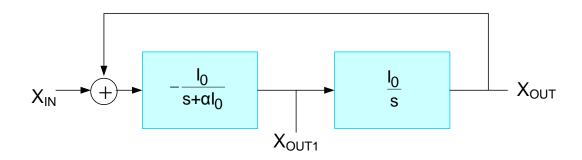
Review from Earlier Lecture Observation

- Many papers have appeared that tout the performance advantages of current-mode circuits
- In all of the current-mode papers that this instructor has seen, no attempt is made to provide a quantitative comparison of the key performance features of current-mode circuits with voltage-mode counterparts
- All justifications of the advantages of the currentmode circuits this instructor has seen are based upon qualitative statements

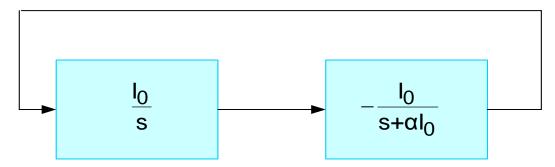
Observations (cont.)

- It appears easy to get papers published that have the term "current-mode" in the title
- Over 900 papers have been published in IEEE forums alone!
- Some of the "current-mode" filters published perform better than other "voltage-mode" filters that have been published
- We are still waiting for even one author to quantitatively show that current-mode filters offer even one of the claimed four advantages over their voltage-mode counterparts

Will return to a discussion of Current-Mode filters later

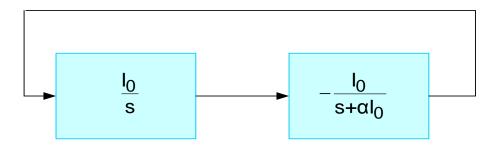


- For notational convenience, the input signal can be suppressed and output will not be designated
- This forms the "dead network"
- Poles for dead network are identical to original network as are key sensitivities

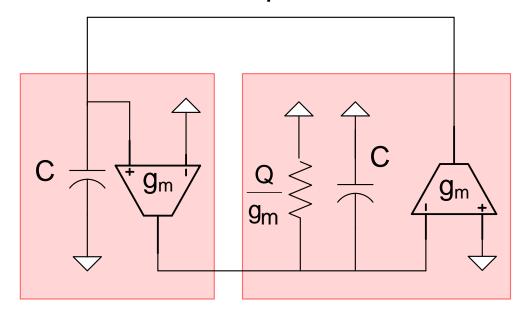


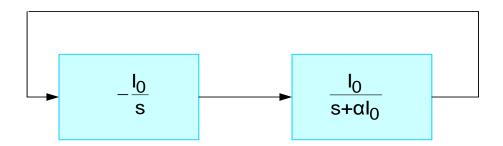
Two Integrator Loop Biquad

OTA-C implementation

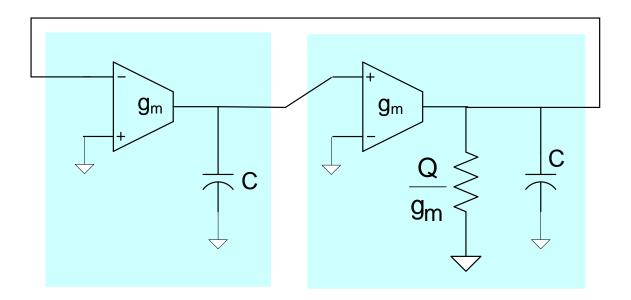


Consider a current-mode implementation:

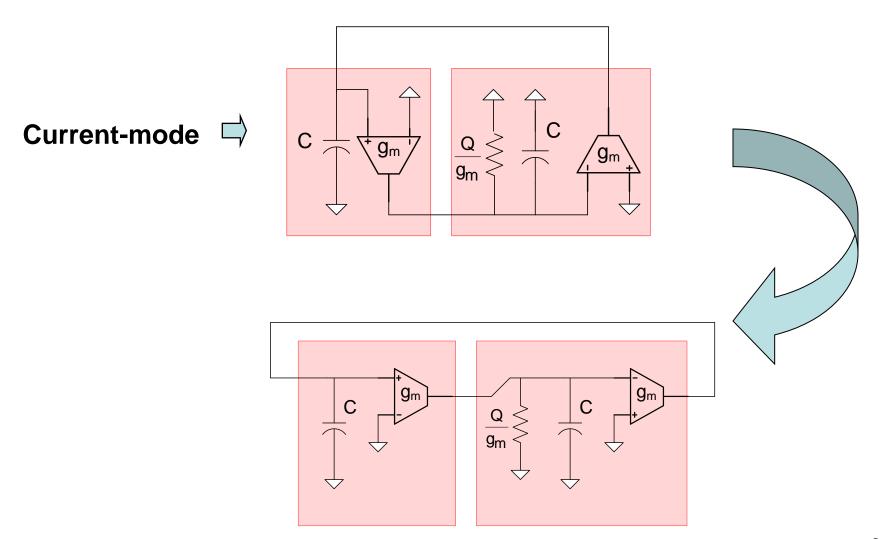


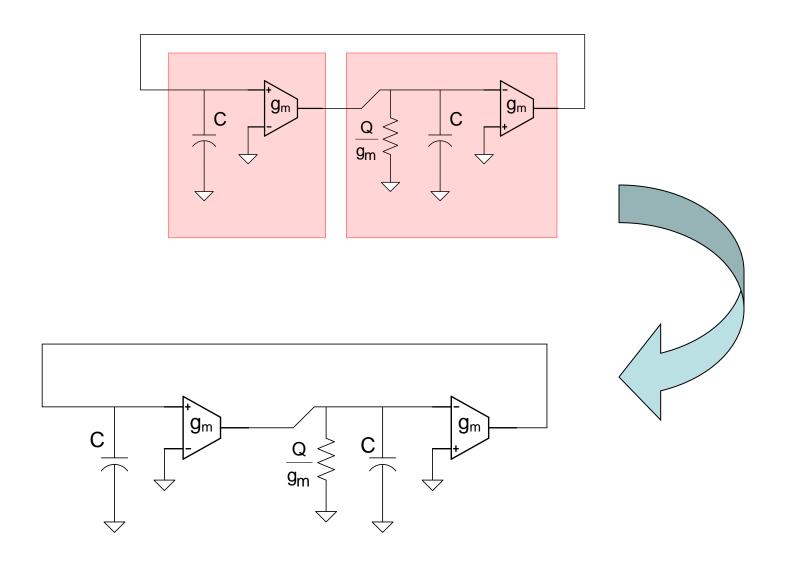


Consider the corresponding voltage-mode implementation:

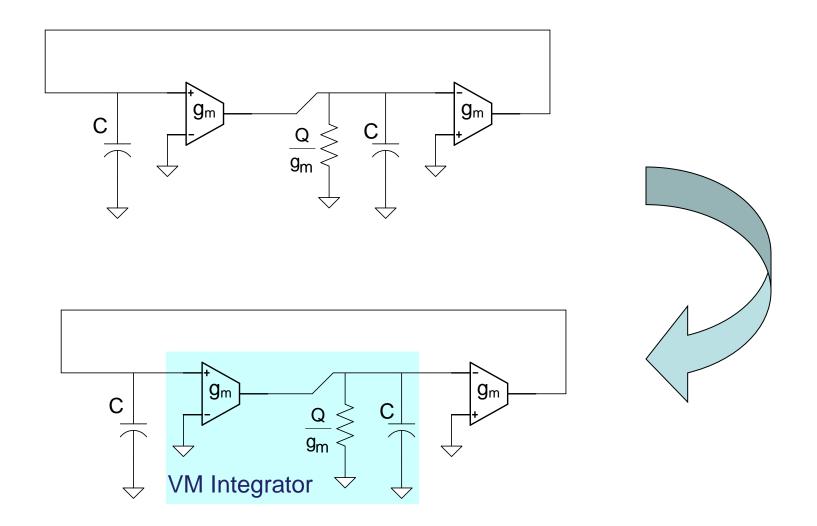


An Observation:

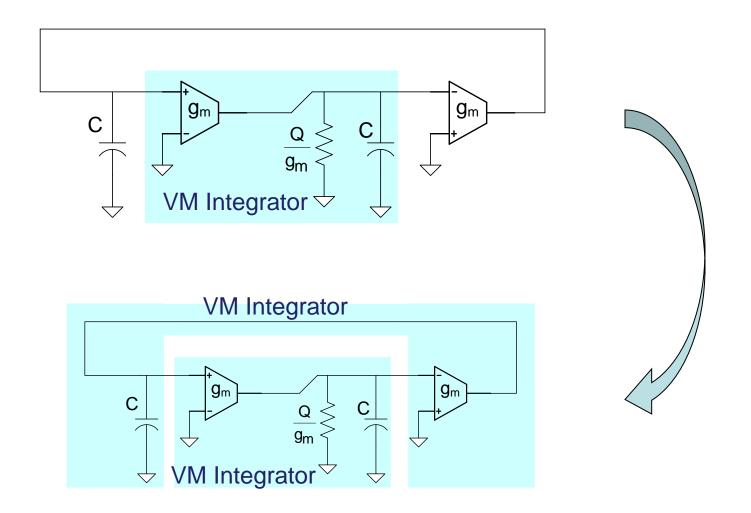




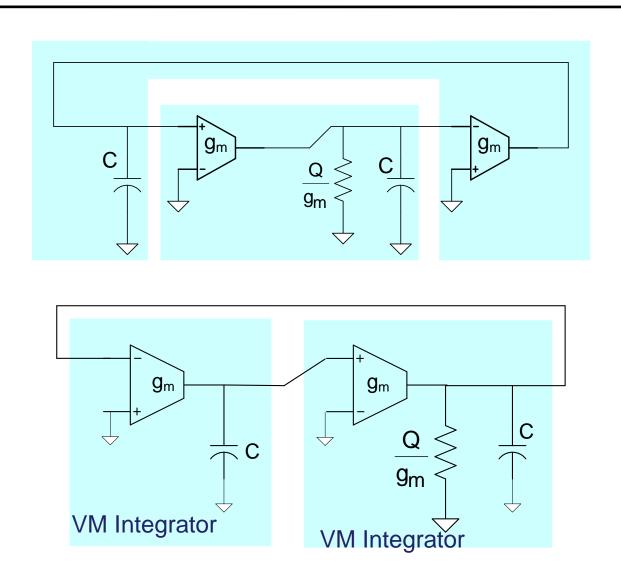
3-08 100

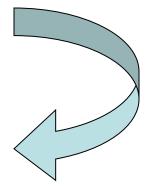


3-08 101



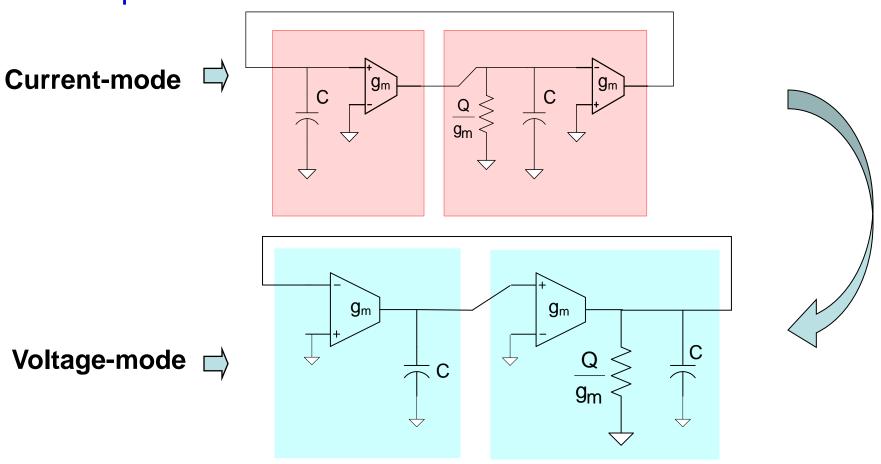
3-08 102





This circuit was well-known in the 80's

OTA-C implementation



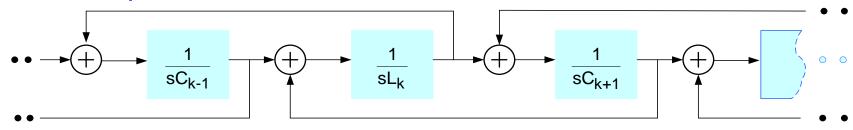
Current-mode and voltage-mode circuits have same component count Current-mode and voltage-mode circuits are identical!

Current-mode and voltage-mode properties are identical!

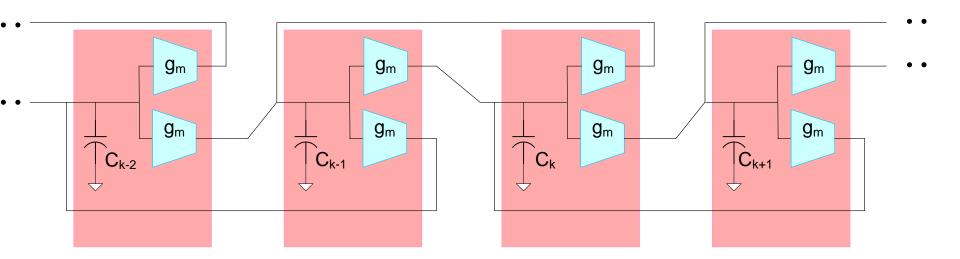
Current-mode circuit offers NO benefits over voltage-mode counterpart

104

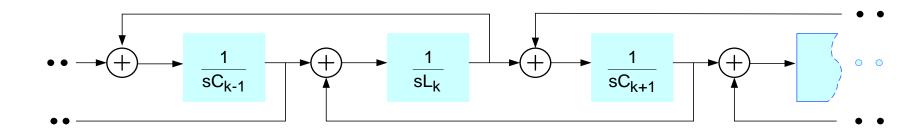
OTA-C implementation



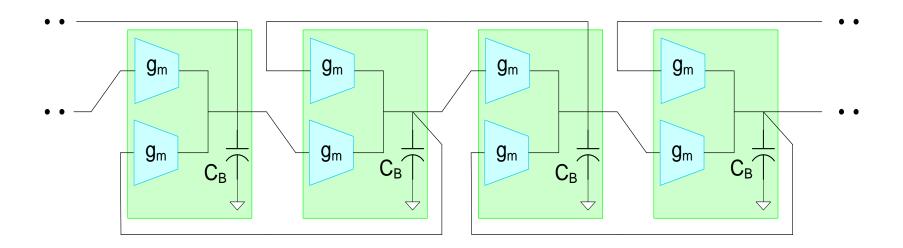
Consider a current-mode implementation:



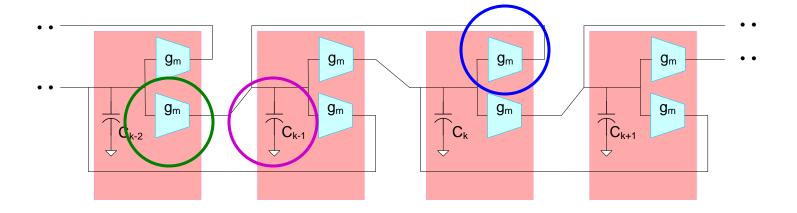
Numerous current-mode filter papers use this basic structure 105



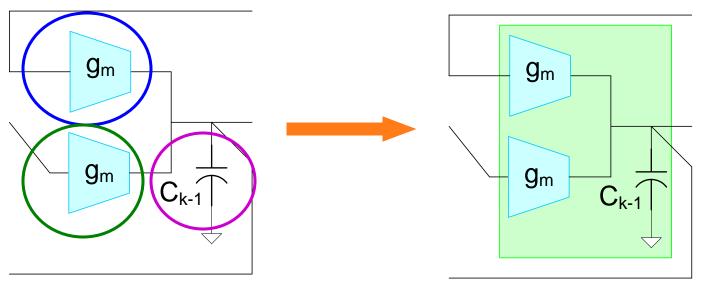
Consider a voltage-mode implementation:



An Observation:

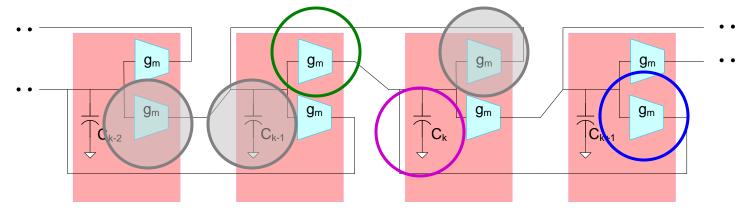


Consider lower OTA in stage k-2, capacitor in stage k-1 and upper OTA in stage k

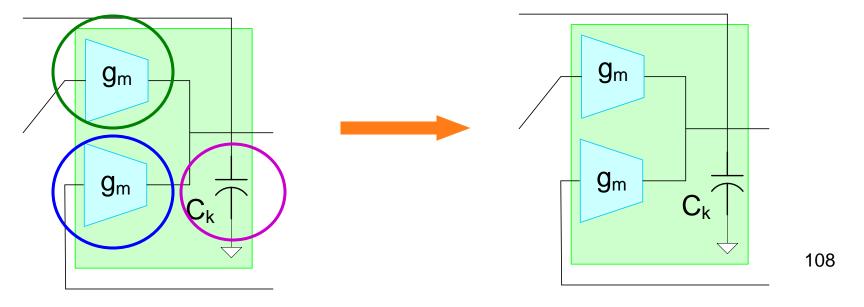


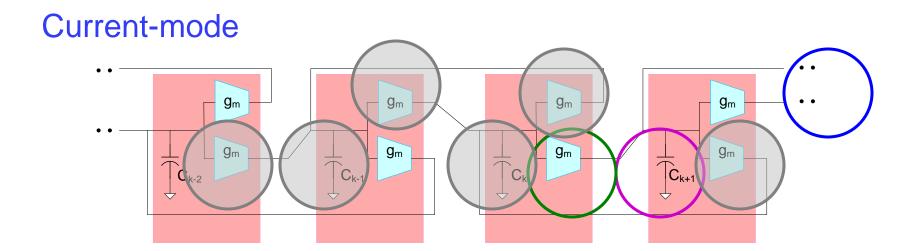
107

Current-mode

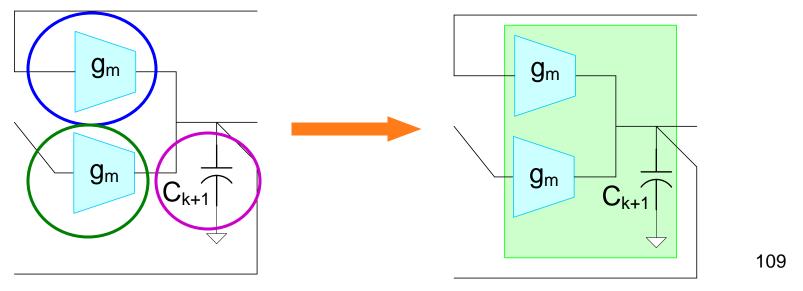


Consider upper OTA in stage k-1, capacitor in stage k and lower OTA in stage k+1

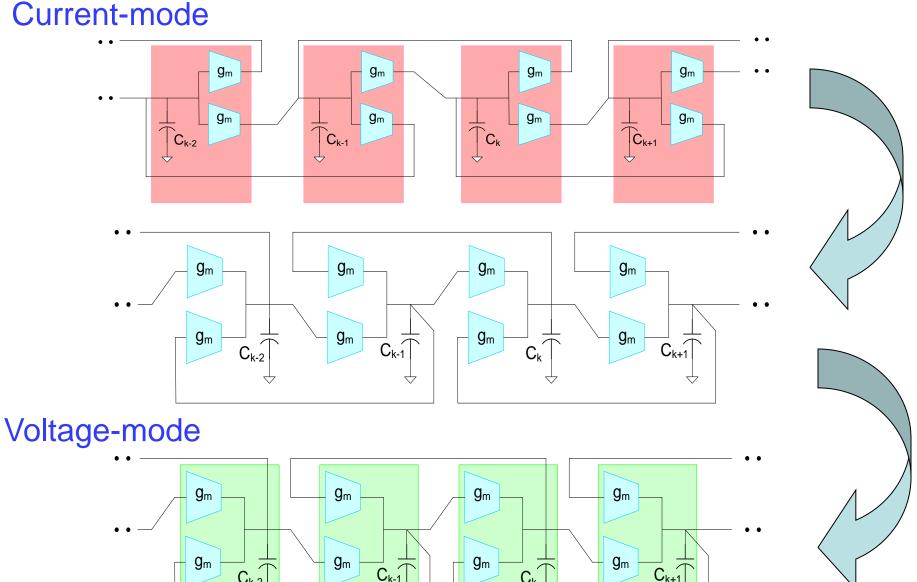




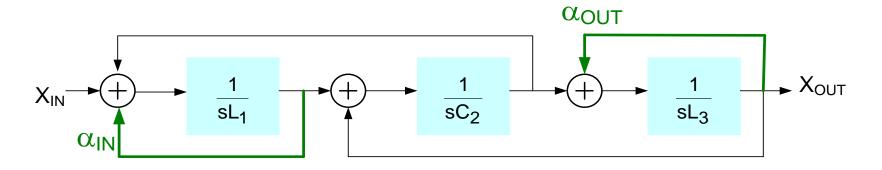
Consider lower OTA in stage k, capacitor in stage k+1 and upper OTA in stage k+2



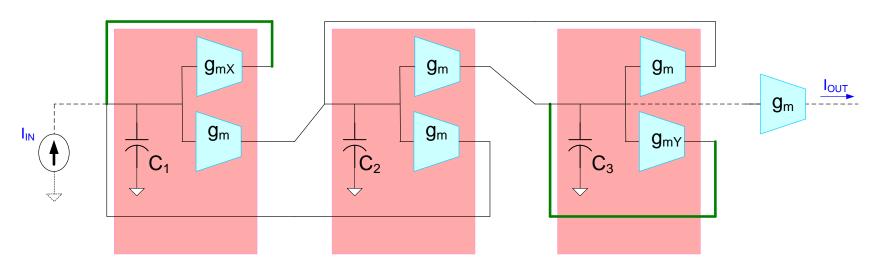
Current-mode



Terminated Leap-Frog Filter (3-rd order lowpass)

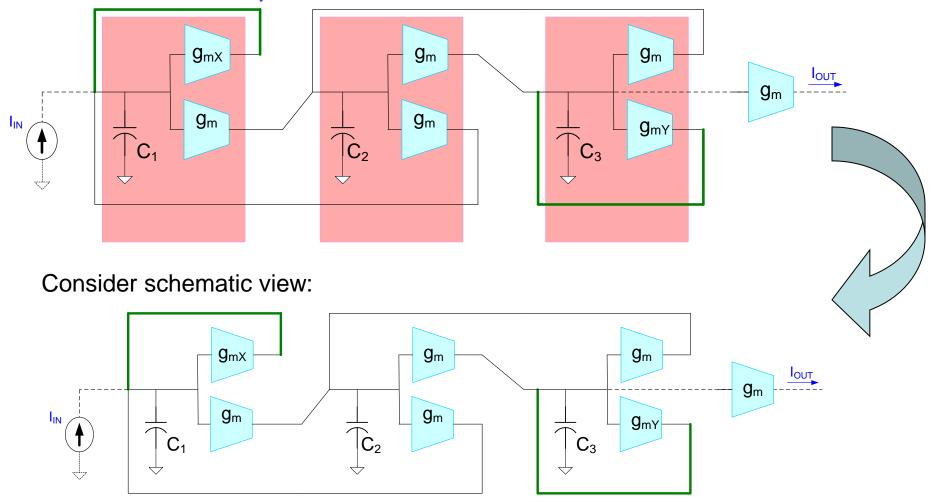


Current-mode implementation



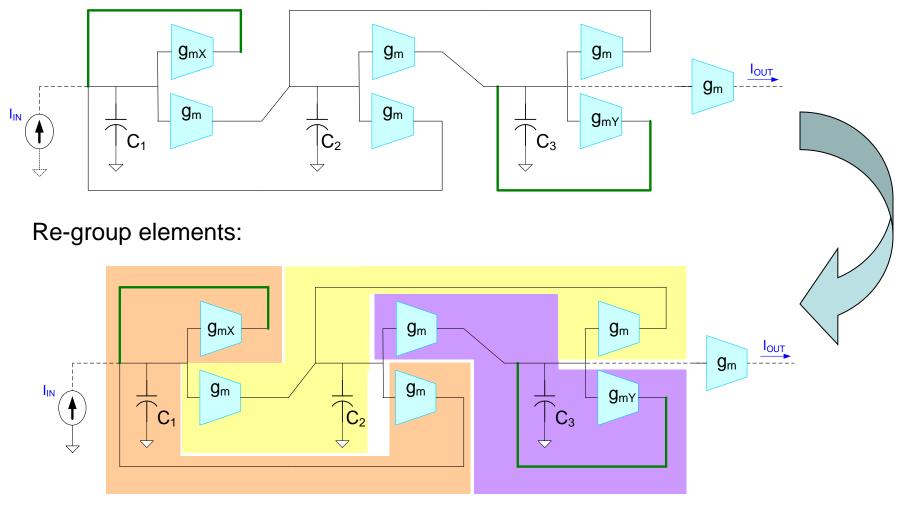
3-08

Current-mode implementation



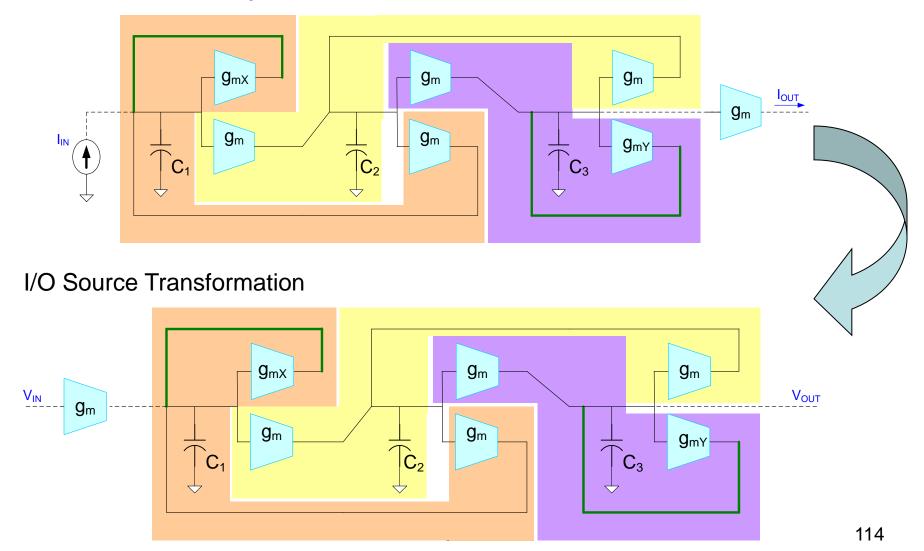
3-08 112

Current-mode implementation

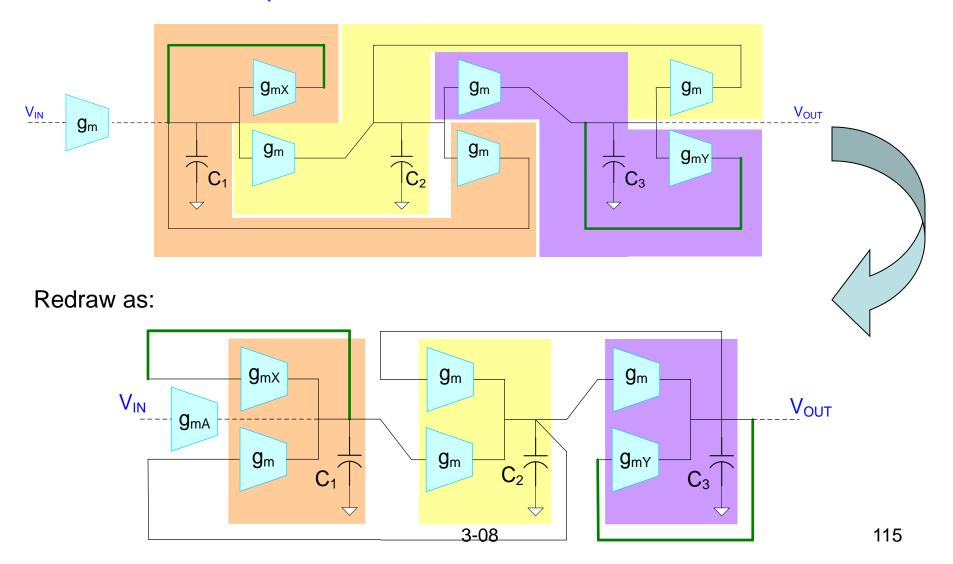


3-08 113

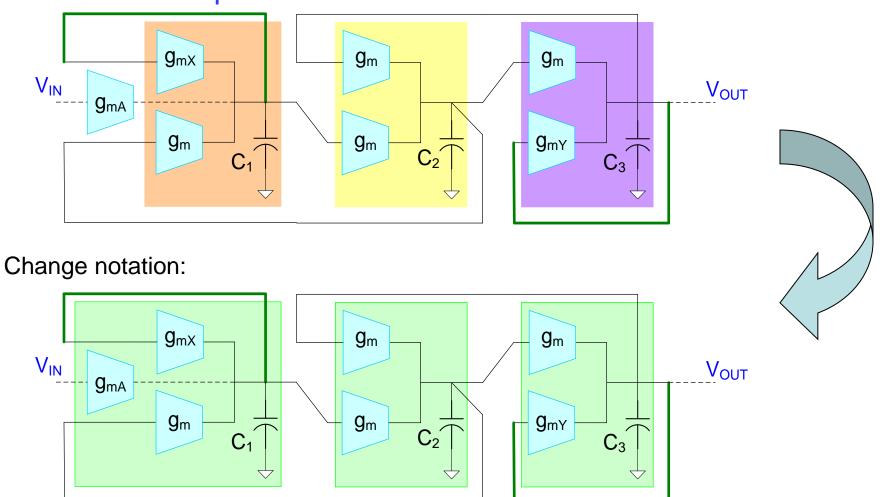
Current-mode implementation

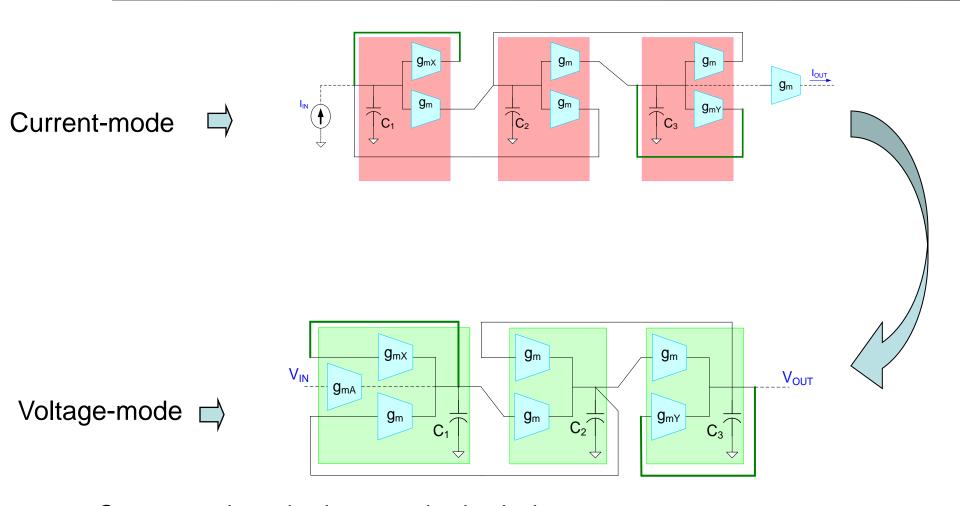


Current-mode implementation



Current-mode implementation





Current-mode and voltage-mode circuits have same component count Current-mode and voltage-mode circuits are identical!

Current-mode and voltage-mode properties are identical!

Current-mode circuit offers NO benefits over voltage-mode counterpart 17

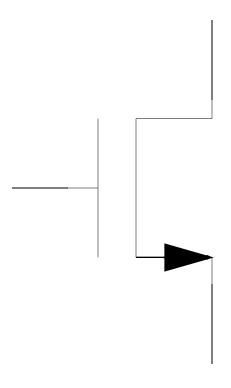
Questions about the Conventional Wisdom

What is a current-mode circuit?

- Everybody seems to know what it is
- Few have tried to define it
- Is a current-mode circuit not a voltagemode circuit?

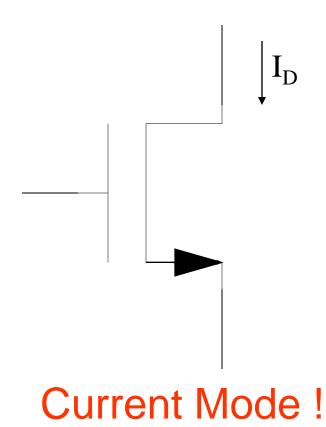
Question?

Is the following circuit a voltage mode-circuit or a current-mode circuit?



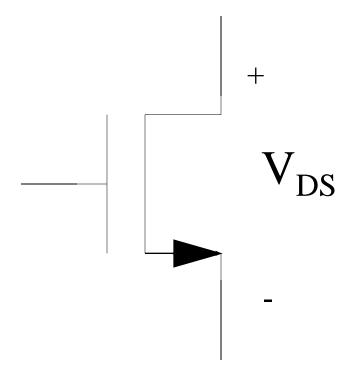
Question?

Is the following circuit a voltage mode-circuit or a current-mode circuit?



Question?

Is the following circuit a voltage mode-circuit or a current-mode circuit?



Voltage Mode!

Observations:

- Voltage-Mode or Current-Mode Operation of a Given Circuit is not Obvious
- All electronic devices have a voltage-current relationship between the port variables that characterizes the device
- The "solution" of all circuits is identical independent of whether voltages or currents are used as the state variables
- The poles of any circuit are independent of whether the variables identified for analysis are currents or voltages or a mixture of the two

Observation

- Conventional wisdom suggests numerous performance advantages of current-mode circuits
- Some of the "current-mode" filters published perform better than other "voltage-mode" filters that have been published
- Few, if any, papers provide a quantitative comparison of the key performance features of current-mode circuits with voltage-mode counterparts
- It appears easy to get papers published that have the term "current-mode" in the title

Observations (cont.)

- Over 900 current-mode papers have been published in IEEE forums alone!
- Most, if not all, current-mode circuits are IDENTICAL to a voltage-mode counterpart
- We are still waiting for even one author to quantitatively show that current-mode filters offer even one of the claimed four advantages over their voltage-mode counterparts

Are Conventional Wisdom and Fundamental Concepts always aligned in the Microelectronics Field?



Will consider 4 basic examples in this discussion

- Op Amp
- Positive Feedback Compensation
- Current Mode Filters



Current Dividers

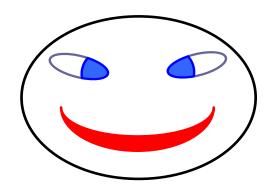


Current Dividers

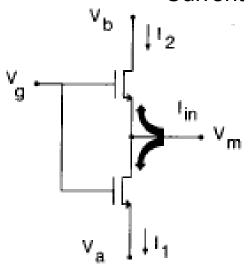
- Background
 - Objective
 - Concept of Current Divider
 - Characterization of Inherently Linear Current Divider
 - Inherent Current Division in Symmetric Circuits
 - Conclusionhs

Current Dividers

Motivation: Circuits that do accurate current division in the presence of varying loading conditions could be among the most useful building blocks that are available



Current divider with "Inherent Linearity"



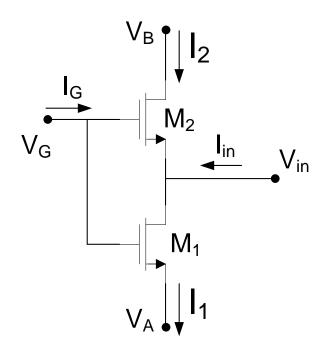
. The basic principle of current division.

- constant and independent of I_{in} (implying low distortion),
- independent of the values of V_a and V_b,
- independent of whether one or both devices are saturated or nonsaturated,
- and also independent of whether one or both devices operate in strong or in weak inversion.

above we have assumed that V_a and V_b are ideal voltage sources, i.e., having zero output impedance.

- Examples that were given did not have zero impedance on V_A and V_B nodes
- Experimentally reported THD from -80dB to -85dB
- Experimentally measured Dynamic Range in excess of 100dB
- All digital standard CMOS process

Bult and Geelen, ISSCC Feb1992, JSC Dec 1992 "An Inherently Linear and Compact MOST-only Current Division Technique"



Current Division Factor

$$\theta = \frac{(W/L)_1}{(W/L)_2}$$

Very Simple and Compact

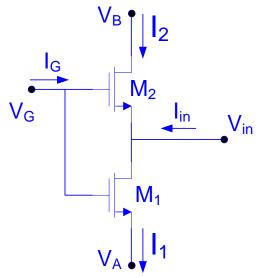
Elegant!



Current divider with "Inherent Linearity"



Bult and Geelen, ISSCC Feb1992, JSC Dec 1992 "An Inherently Linear and Compact MOST-only Current Division Technique"

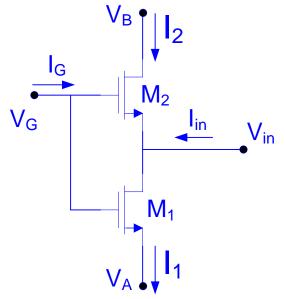


Inherently Linear Current Divider



Conventional Wisdom: current division factor independent of

- $-I_{IN}$
- $-V_A$ and V_B
- Device operation region (weak, moderate, or strong inversion; triode or saturation region)
- body effect, mobility degradation



Inherently Linear Current Divider

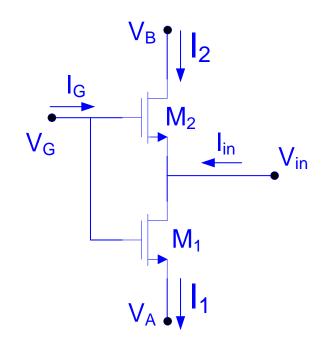
only weakly dependent upon second-order effects

THD better than -85dB in audio range Dynamic Range better than 100dB Experimentally verified

Very impressive linearity properties!

Influential Concept

- Outstanding paper of ISSCC 1992
- Cited 180 times Google Scholar
- Reported applications include
 - Volume controller
 - Data converter
 - Tunable filters
 - Variable gain amplifier
 - Accurate current generator
 - Sensors
 - Other circuits
- Numerous reported works experimentally verify the high linearity



Inherently Linear Current Divider

An example application of the concept and the circuit

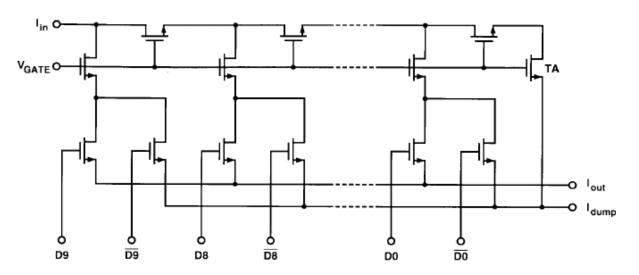
IEEE JOURNAL OF SOLID-STATE CIRCUITS, VOL. 33, NO. 8, AUGUST 1998



Design and Implementation of an Untrimmed MOSFET-Only 10-Bit A/D Converter with -79-dB THD

Clemens M. Hammerschmied, Student Member, IEEE, and Qiuting Huang, Senior Member, IEEE

The MOSFET ladder is based on a linear current division principle instead, the basic circuit of which is depicted in Fig. 4 [14]. An input current $I_{\rm in}$ is divided into two currents



40 Google Scholar Citations (Dec. 15, 2010)

An example application of the concept and the circuit

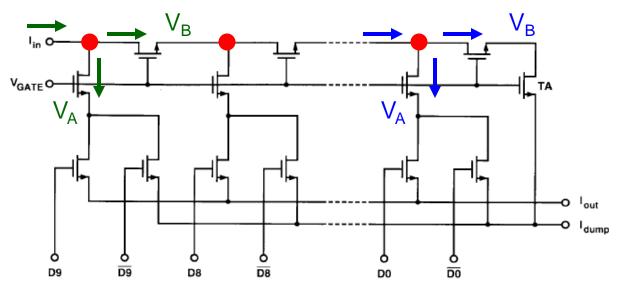
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The MOSFET ladder is based on a linear current division principle instead, the basic circuit of which is depicted in Fig. 4 [14]. An input current $I_{\rm in}$ is divided into two currents



V_A and V_B not even at zero impedance nodes!

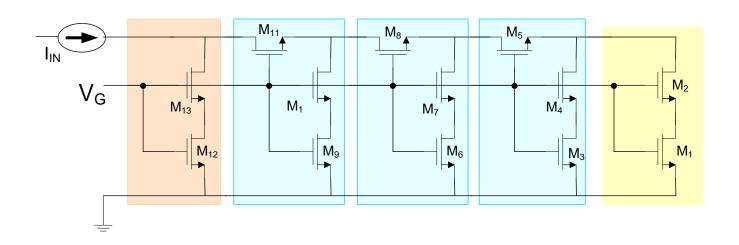
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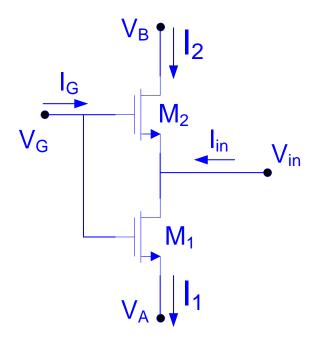
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But



Inherently Linear Current Divider

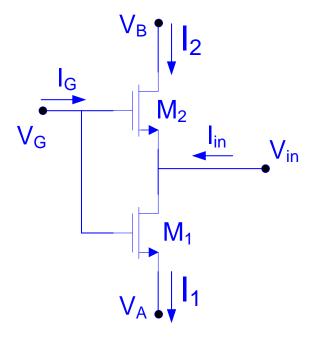
We have been unable to achieve linearity that is even close to that reported in different but closely related applications of this circuit

(e.g. -40dB or less linearity in contrast to -85dB or better performance)

Outline

- Background
- Objective
 - Concept of Current Divider
 - Characterization of Inherently Linear Current Divider
 - Inherent Current Division in Symmetric Circuits
 - Conclusionhs

Purpose of this work



Clarify and quantify the potential and limitations of the "inherently linear current divider"

(Do not question the reported experimental results attributed to this circuit)

Current Dividers

- Background
- Objective
- Concept of Current Divider
 - Characterization of Inherently Linear Current Divider
 - Inherent Current Division in Symmetric Circuits
 - Conclusionhs

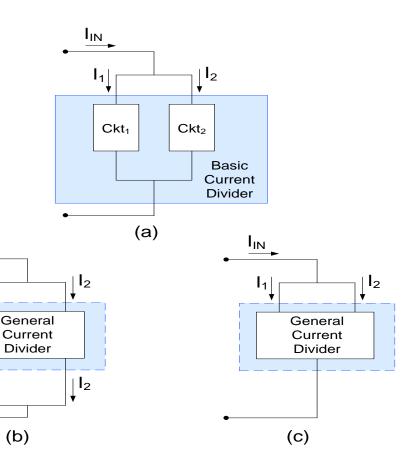
Concept of Current Divider

 I_1

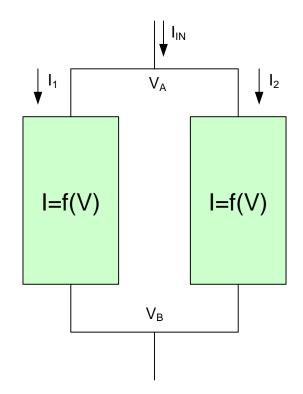
What is a current divider?

- Although the term is widely used, formal definitions seldom if ever given
- Consider a node with three incident branches in a circuit
- If the current in one of the three branches is proportional to that in another branch, we will define this circuit to be a current divider

$$I_1 = \Theta I_{IN}$$



Observations That Will Become Relevant



$$\boldsymbol{I_1} = \frac{1}{2}\boldsymbol{I_{IN}}$$

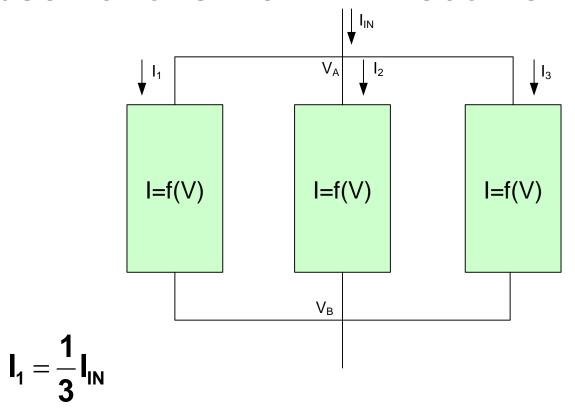
Independent of V_A, V_B, I_{IN.}, f

Inherent property of symmetric network

Current Divider!

Concept that has probably been known for well over 100 years

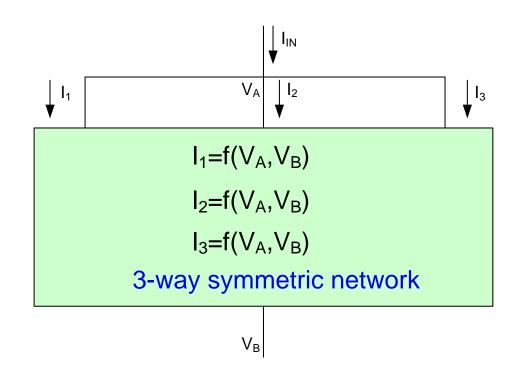
Observations that Will Become Relevant



Independent of V_A , V_B , $I_{IN,}$, f

Inherent property of symmetric network

Observations that Will Become Relevant



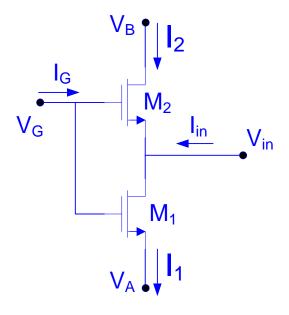
$$I_1 = \frac{1}{3}I_{IN}$$

Independent of V_A, V_B, I_{IN}, f

Inherent property of symmetric network

Concept that has probably been known for well over 100 years

Consider the Inherently Linear Current Divider with Linearity Challenges



Conventional Wisdom: current division factor independent of

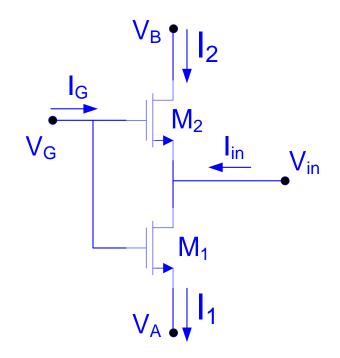
- $-I_{IN}$
- $-V_A$ and V_B
- Device operation region (weak, intermediate, or strong inversion; triode or saturation region of operation)
- body effect, mobility degradation

Current Dividers

- Background
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Assumptions

- Square-law model
- Identical V_{th}
- No Body or Output
 Conductance Effects
- {I_{in}, V_{GA}, V_{BA}} independent variables



$$\eta_1 = \mu C_{OX}(W_1/L_1)$$

 $\eta_2 = \mu C_{OX}(W_2/L_2)$

From a straightforward but tedious analysis

If M₁ in the triode region and M₂ in the triode region

$$\begin{split} \textbf{I}_{1} &= \boxed{\frac{\eta_{1}}{\eta_{1} + \eta_{2}}} \, \textbf{I}_{in} + \frac{\eta_{1}\eta_{2}}{\eta_{1} + \eta_{2}} \, \textbf{V}_{BA} \left(\textbf{V}_{GA} - \textbf{V}_{T} - \frac{\textbf{V}_{BA}}{2} \right) \\ \textbf{V}_{inA} &= \textbf{V}_{GA} - \textbf{V}_{T} - \sqrt{(\textbf{V}_{GA} - \textbf{V}_{T})^{2} - 2 \left(\left[\frac{1}{\eta_{1} + \eta_{2}} \right] \textbf{I}_{in} + \frac{\eta_{2}}{\eta_{1} + \eta_{2}} \, \textbf{V}_{BA} \left(\textbf{V}_{GA} - \textbf{V}_{T} - \frac{\textbf{V}_{BA}}{2} \right) \right) \end{split}$$

Oddly, the driving point voltage is dependent upon the driving point current!

From a straightforward but tedious analysis

If M₁ in the triode region and M₂ in the saturation region

$$I_{1} = \frac{\eta_{1}}{\eta_{1} + \eta_{2}} I_{in} + \frac{\eta_{1}\eta_{2}}{2(\eta_{1} + \eta_{2})} (V_{GA} - V_{T})^{2}$$

$$V_{inA} = (V_{GA} - V_{T}) \left(1 - \sqrt{\frac{\eta_{1} - \frac{2I_{in}}{(V_{GA} - V_{T})^{2}}}{\eta_{1} - \eta_{2}}}\right)$$

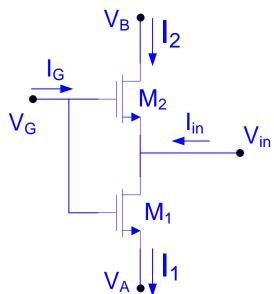
Oddly, the driving point voltage is dependent upon the driving point current!

From a straightforward but tedious analysis using the basic square-law model

If V_{GA} and V_{GB} do not depend upon I_{IN} , then

- the circuit performs as a linear current divider with an offset
- the current divider ratio does not change as M₁ and
 M₂ change from the triode region to the saturation region

But, if these conditions are not satisfied, will the circuit still perform as a linear current divider?



Some things ignored in previous analysis

- Device model errors (not exactly square-law)
- Threshold voltages mismatches
- Finite output impedance of transistors
- Body effect
- Finite output impedance of the current source

More Accurate Analysis

- Analytical study is unwieldy with highly complicated model
- Computer simulation helpful for predicting linearity

Linearity Metrics

Static linearity defined as deviation from fit line

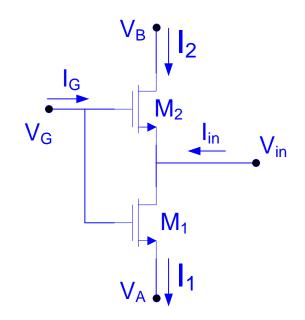
$$I_{1FIT}(I_{in}) = I_{1Q} + \frac{\partial I_{1}}{\partial I_{in}} \Big|_{\{I_{inQ}, V_{GAQ}, V_{inAQ}\}} \cdot (I_{in} - I_{inQ})$$

$$\Delta = \left[\frac{I_1(I_{in}) - I_{1FIT}(I_{in})}{I_{1FIT}(I_{in})} \right] \times 100\%$$

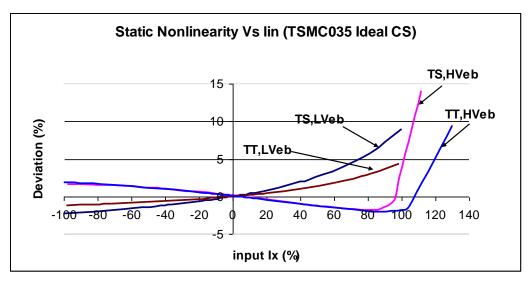
Dynamic linearity defined as the THD performance with continuous sinusoid excitation

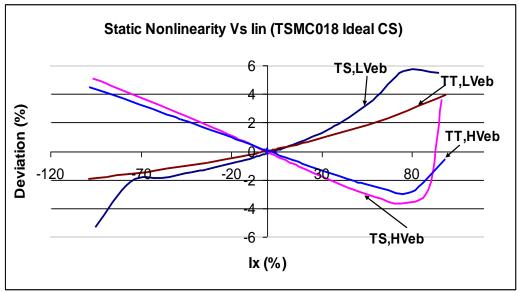
Simulation Environments

- Different operation regions (M₁, M₂)
 - Triode, Triode ("TT")
 - Triode, Saturation ("TS")
- Different bias level
 - Large V_{EB}
 - Small V_{FB}
- Different size devices (width, length)
- Different process
 - TSMC 0.18um
 - TSMC 0.35um
- V_{AS}, V_{BS}, V_{GS} fixed
- Ideal current source excitation

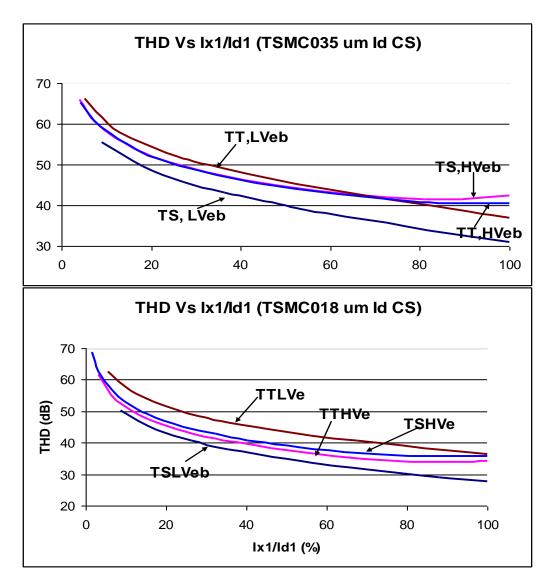


Static Linearity Simulation





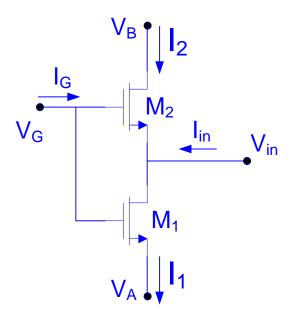
Dynamic Linearity Simulation



Observations about Linearity

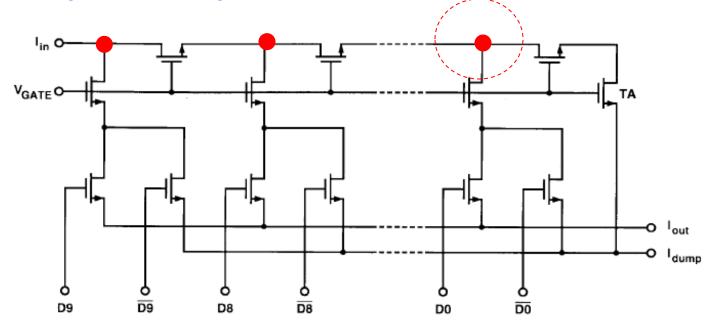
- Static nonlinearity in the few percent range
- Dynamic linearity is quite limited with even moderate input current levels
 - limited to about 30~40 dB level if reasonable input current swings occur
- Including effects of output impedance of current source and circuit dependence of V_{AS} and V_{BS} will further degrade performance

Observations about inherently linear current divider



- Performance as a current divider is somewhat questionable
- Not inherently linear (appears to be strongly dependent upon model)

Consider again the Huang circuit (in which all transistors are identical)



For proper operation, it is critical that currents divide equally at each of The current division nodes!

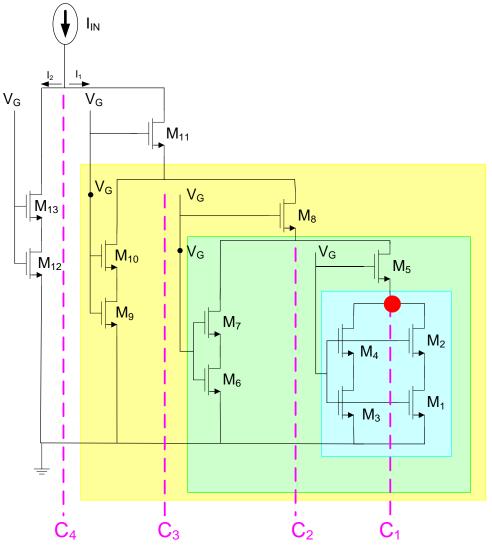
Even the assumption that the voltages V_A and V_B must be zero-impedance sources was not required to obtain the good performance (79 dB range)!

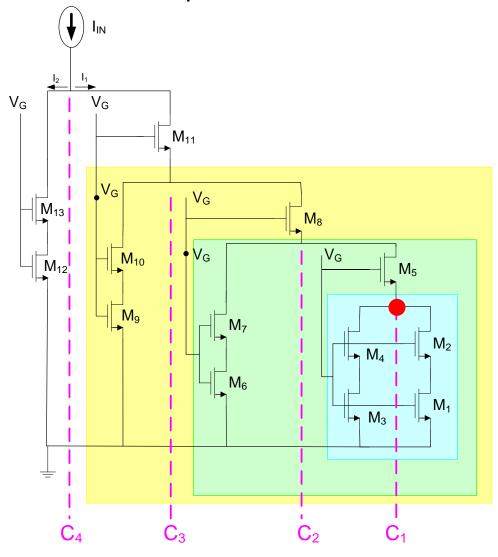
Question: How was the excellent linearity obtained in the author's own work and that reported in the literature if it is difficult to verify the linearity?

Redraw the Huang Circuit and Consider the right-most

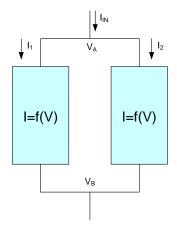
Redraw the Huang Circuit and Consider the right-most

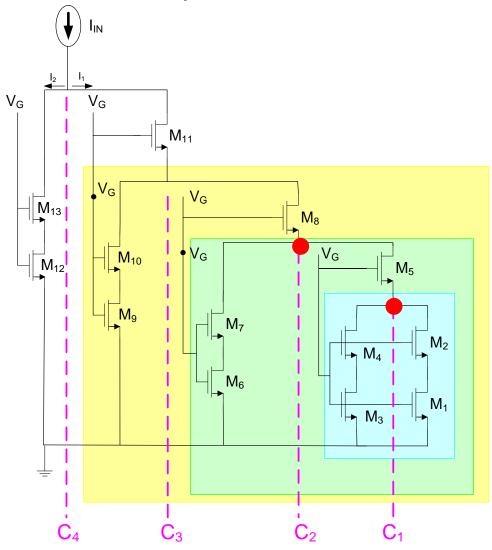
Current Divider node



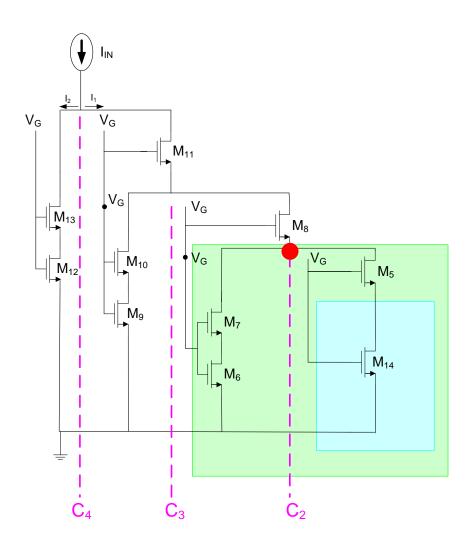


- Circuit in blue is completely symmetric on C₁ and is the well-known current divider
- it is not dependent upon any specific properties of the transistors!
- This was the right-most node where the "inherently linear" current divider was used!

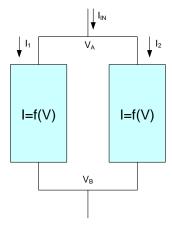


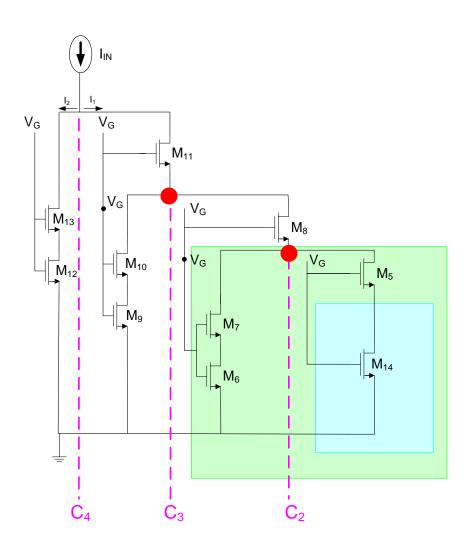


- Observe that M₁,M₂,M₃,M₄ can be modeled as a single transistor that is of the same size as M₁
- Call this M₁₄
- Consider now the next closest current-divider node

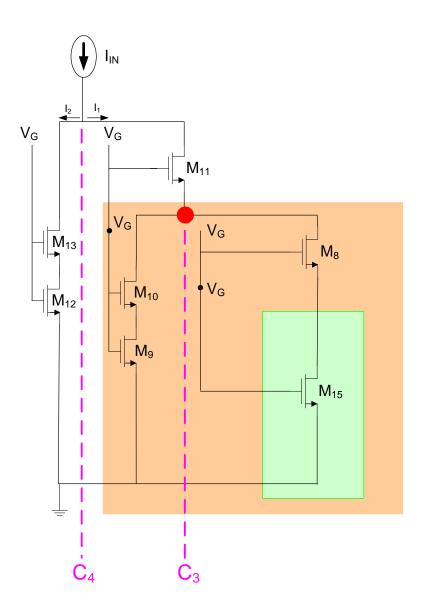


- Circuit in green is completely symmetric about C₂ and is the well-known current divider
- it is not dependent upon any specific properties of the transistors!

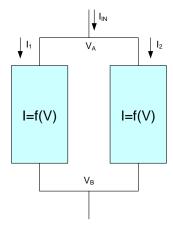


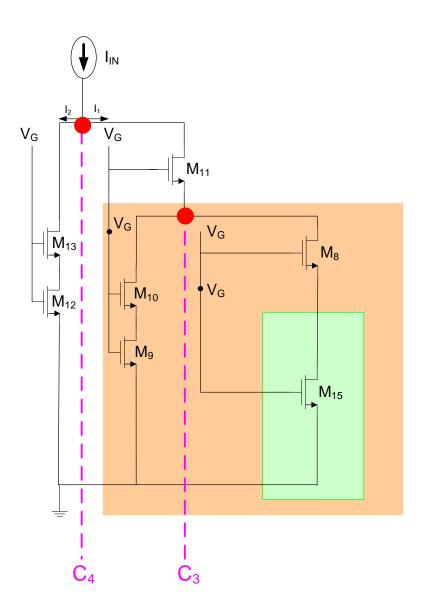


- Observe that M_6 , M_7 , M_5 , M_{14} can be modeled as a single transistor that is of the same size as M_1
- Call this M₁₅
- Consider now the next closest current-divider node

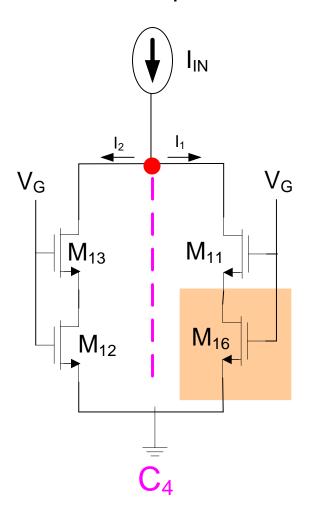


- Circuit in brown is completely symmetric on C₃ and is the well-known current divider
- it is not dependent upon any specific properties of the transistors!

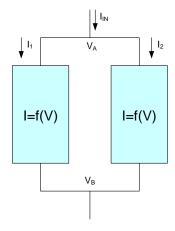




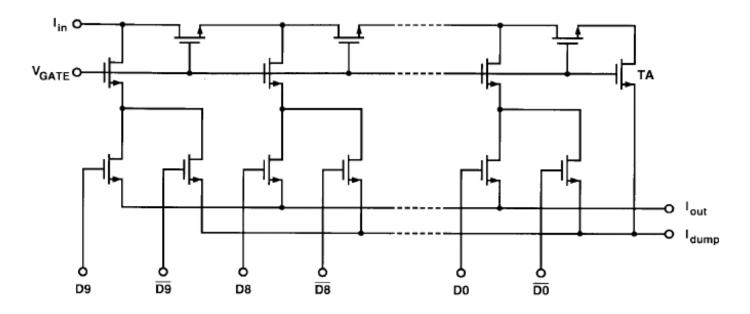
- Observe that M_9, M_{10}, M_8, M_{15} can be modeled as a single transistor that is of the same size as M_1
- Call this M₁₆
- Consider now the next closest current-divider node



- Circuit shown is completely symmetric on C₃ and is the well-known current divider
- it is not dependent upon any specific properties of the transistors!



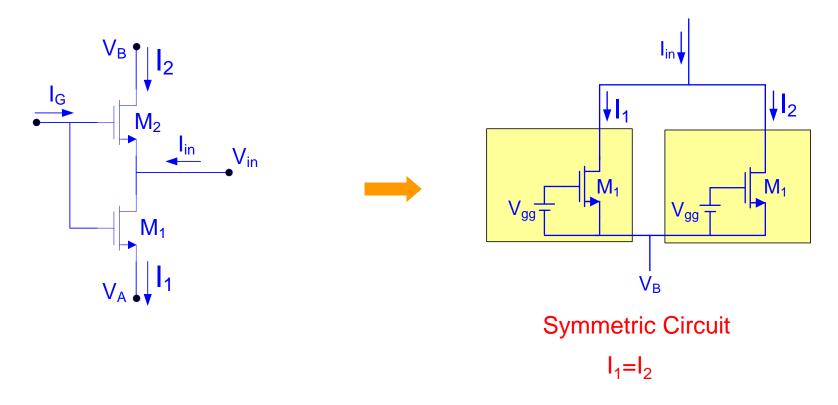
Current divider properties of the Huang DAC (ADC) were all dependent upon the general current division property of symmetric networks and had nothing to do with the current division in two transistors!



Current divider properties of the experimentally reported work of the original author were all dependent upon the general current division property of symmetric networks and had nothing to do with the current division in two transistors!

How was the very good performance of the "inherently linear" current divider obtained?

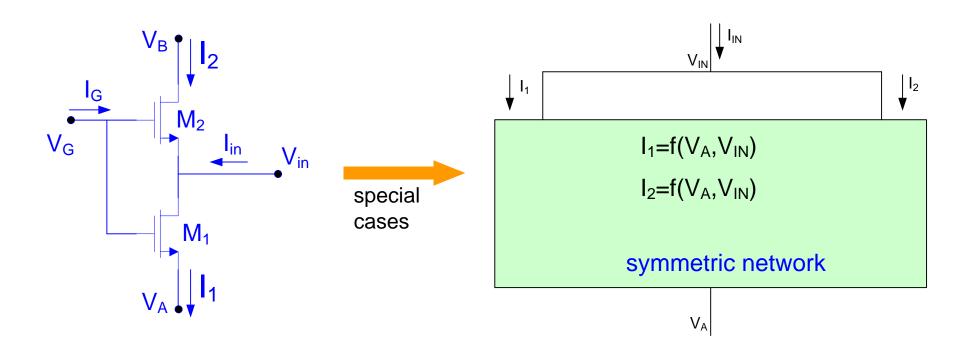
About 12 months ago one of our Ph.D. students looked at all SCI citations that referenced the "inherently linear" current divider and the performance in all cases was a special case of the general symmetric circuit



Current Dividers

- Background
- Objective
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- Inherent Current Division in Symmetric Circuits
 - Conclusionhs

Good linearity properties of "inherently linear" current divider for those we found in the literature are due to well-known symmetry properties of circuits, not due to unique properties of the two-transistor current-divider structure



Conclusion

- The linearity properties are not apparent with existing device models
- Based upon existing models, operation as a current divider in question and linearity can be orders of magnitude worse than previously reported
- Good linearity properties of all applications found in literature survey for this circuit are due to well-known symmetry properties, not inherent characteristics of the two-transistor structure
- Experimental evidence appears to be lacking to support the inherently linearity properties of the current divider
- Is it possible that the circuit performs as an inherently linear current divider that has not yet been experimentally verified?
- Is it possible that there are major errors in existing device models used in circuit simulators that cause dramatic linearity errors in the simple 2-transistor current divider?

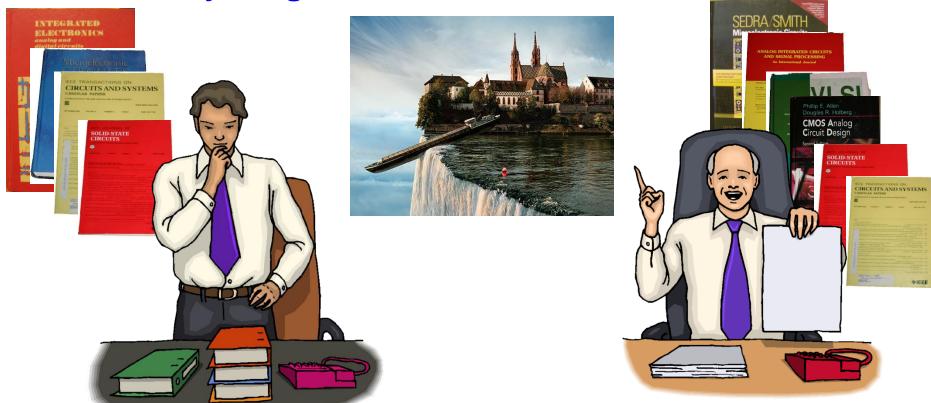
Are Conventional Wisdom and Fundamental Concepts always aligned in the Microelectronics Field?



Just considered conventional wisdom in 4 basic examples

- Op Amp
- Positive Feedback Compensation
- Current Mode Filters
- Current Dividers

Are Conventional Wisdom and Fundamental Concepts always aligned in the Microelectronics Field?



Four examples involving some of the most basic concepts in the microelectronics field were identified where the alignment of conventional wisdom and fundamental concepts are weak

Many more examples exist where alignment is weak

Are Conventional Wisdom and Fundamental Concepts always aligned in the Microelectronics Field?





Conventional Wisdom is VERY USEFUL for enhancing productivity and identifying practical approaches to engineering design and problem solving

Conventional Wisdom, however, should not be viewed as a basic principle or fundamental concept

Keep an OPEN MIND when using Conventional Wisdom to recognize both the benefits and limitations and recognize that even some of the most reputable sources and reputable engineers/scholars do not always distinguish between conventional wisdom and fundamental concepts

Thank you for your attention!

End of Lecture 44